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# RESEARCH MEMORANDUM

WIND-TUNNEL INVESTIGATION AT SUBSONIC AND SUPERSONIC SPEEDS OF A  
MODEL OF A TAILLESS FIGHTER AIRPLANE EMPLOYING A LOW-ASPECT-  
RATIO SWEEPED-BACK WING - EFFECTS OF EXTERNAL FUEL TANKS  
AND ROCKET PACKETS ON THE DRAG CHARACTERISTICS

By Willard G. Smith

Ames Aeronautical Laboratory  
Moffett Field, Calif.

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

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AND ROCKET PACKETS ON THE DRAG CHARACTERISTICS

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SUMMARY

The effects of external fuel tanks and externally mounted rocket packets on the drag characteristics of a model of a tailless fighter airplane are presented in this report. The investigation was conducted through a Mach number range of 0.60 to 0.90 and 1.20 to 1.70 at a constant Reynolds number of 3.2 million. The measured lift, drag, pitching-moment, and rolling-moment coefficients and lift-drag ratios are presented in tabular form and the drag characteristics and lift-drag ratios are also presented in graphic form. In addition, pressure distribution data are tabulated which may be used to determine the influence of the external stores on the wing load distribution at supersonic speeds.

Results of this investigation show that the addition of two external fuel tanks and four faired rocket packets to the model produced drag increments which increased from 30 percent to 50 percent of the drag of the basic model between Mach numbers of 0.60 and 0.90, respectively, while at supersonic Mach numbers this drag increment was approximately 30 percent of the drag of the basic model. Tests of the model fitted with four rocket packets indicate that the drag may be reduced at subsonic speeds by fairing the open rocket packets, but at supersonic speeds the faired packets produced more drag. A small decrease in drag was realized at supersonic speeds, for the model fitted with two fuel tanks and four rocket packets, by mounting the outboard packets and fuel tanks in a more forward chordwise position with respect to the wing.

INTRODUCTION

Knowledge of the increases in drag to be expected from the addition of externally mounted fuel tanks and armament under the wings and fuselage becomes increasingly important as the trend continues toward long-range, high-speed fighter airplanes carrying rocket-propelled armament. An

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investigation of the effects of this type of external installation on the aerodynamic characteristics of a model having a low-aspect-ratio swept-back wing has been conducted in the Ames 6- by 6-foot supersonic wind tunnel. The model was fitted with various combinations of under-the-wing type rocket-packet and fuel-tank installations and tested at subsonic and supersonic Mach numbers at a constant Reynolds number. Two chordwise locations of the fuel tanks and rocket packets were investigated and the rocket packets were tested with the ends of the packets faired smooth and with the rocket tubes open. The results of this investigation are presented herein. The results of an investigation of the stability and control characteristics of this same model conducted in the Ames 6- by 6-foot supersonic wind tunnel are presented in reference 1.

#### NOTATION

The lift, drag, and pitching-moment coefficients are referred to the stability axes with the origin at the quarter-chord point of the mean aerodynamic chord projected to the fuselage center line. Rolling-moment coefficients are referred to the fuselage longitudinal axis.

b	wing span, feet
c	local wing chord measured parallel to plane of symmetry, feet
$\bar{c}$	wing mean aerodynamic chord $\left( \frac{\int_0^{b/2} c^2 dy}{\int_0^{b/2} c dy} \right)$ , feet
$C_D$	drag coefficient $\left( \frac{\text{drag}}{qS} \right)$
$C_{D_B}$	increment of drag coefficient due to external-store installation or fuselage modification based on total wing area ( $C_{D_{\text{model}}} + \text{store} - C_{D_{\text{model}}}$ )
$C_L$	lift coefficient $\left( \frac{\text{lift}}{qS} \right)$
$C_l$	rolling-moment coefficient $\left( \frac{\text{rolling moment}}{qSb} \right)$
$C_m$	pitching-moment coefficient $\left( \frac{\text{pitching moment}}{qS\bar{c}} \right)$
$C_p$	static pressure coefficient $\left( \frac{p-p_o}{q} \right)$
$\frac{L}{D}$	lift-drag ratio

$\left(\frac{L}{D}\right)_{\max}$	maximum lift-drag ratio
M	free-stream Mach number
p	local static pressure, pounds per square foot
p <sub>0</sub>	free-stream static pressure, pounds per square foot
q	free-stream dynamic pressure, pounds per square foot
R	Reynolds number, based on the mean aerodynamic chord
S	total projected wing area, including area formed by extending leading and trailing edges to plane of symmetry, square feet
Y	spanwise distance from plane of symmetry, feet
$\alpha$	angle of attack of fuselage longitudinal axis, degrees

## APPARATUS

### Wind Tunnel and Equipment

The present investigation was conducted in the Ames 6- by 6-foot supersonic wind tunnel. This is a closed-return, variable-pressure wind tunnel in which the pressure and Mach number can be continuously varied. The stagnation pressure can be varied from 2 to 17 pounds per square inch absolute and the Mach number can be varied from 0.60 to 0.90 and from 1.15 to 2.00. A complete description of the wind tunnel is given in reference 2.

The model was sting mounted with the pitch plane of the model horizontal in the wind tunnel to utilize the most uniform stream conditions. (See reference 2). A four-component electrical strain-gage balance, similar in design to that used in reference 3, was enclosed within the fuselage of the model. The aerodynamic forces and moments were registered by recording-type galvanometers calibrated by applying known loads to the balance.

### Model

A model of a high-speed fighter airplane having a low-aspect-ratio, swept-back wing and a swept-back vertical tail but not horizontal tail was used in this investigation (fig. 1). A bubble-type canopy was faired into a dorsal fin which extended back to the vertical tail. Provisions

were made for fairing the vertical tail into the fuselage when the canopy and dorsal fin were removed. The wing had a leading-edge sweep angle of  $52.5^\circ$  and a taper ratio of 0.332 based on the theoretical wing tip. The wing was composed of symmetrical sections in streamwise planes having a thickness of 7.0 percent of the chord at the wing root tapering to 4.5 percent of the chord at the theoretical wing tip.

The model was fitted with inlets housed in wing-body juncture fairings with internal ducts allowing the air to flow through and exhaust at the rear of the fuselage. In this investigation the mass flow of air through the ducts was not adjustable; however, the ducts were constructed so that at supersonic speeds the exit was choked, limiting the inlet Mach number to 0.4. In order to accommodate the annular duct exit and the mounting sting, the boattailing on the model was somewhat less than would be expected on a full-scale airplane.

Rocket packets and fuel tanks were provided, to be attached to the wings in the locations shown in figures 2 and 3. The outboard rocket packets and the fuel tanks were mounted on unswept and swept-forward pylons as shown in figures 2 and 3. The purpose of the swept-forward pylons was to obtain a more forward location of these stores. The rocket packets were tested both with the fore and aft ends of the rocket packet faired smooth and with six holes open through the packet, to simulate conditions before and after firing the rockets.

Provisions were made to measure pressure distribution data at five spanwise stations as shown in figure 4. The location of the orifices on the upper and lower surfaces of the port wing are given in table I.

#### TESTS AND PROCEDURE

As a basis for comparison, tests were made of the basic model with canopy and dorsal fin in place and with no external stores installed. Lift, drag, pitching-moment, and rolling-moment data were obtained at Mach numbers of 0.60, 0.80, 0.90, 1.20, 1.35, 1.50, and 1.70 at a constant Reynolds number of 3.2 million, through an angle of attack range of  $-2^\circ$  to  $+8^\circ$ . Similar data were then obtained at corresponding test conditions for the following model configurations:

1. Basic model fitted with inboard and outboard faired rocket packets mounted on unswept pylons
2. Basic model fitted with inboard and outboard open-tube rocket packets mounted on unswept pylons
3. Basic model fitted with two external fuel tanks mounted on unswept pylons

4. Basic model fitted with inboard and outboard faired rocket packets and two external fuel tanks all mounted on unswept pylons
5. Basic model fitted with outboard faired rocket packets and two external fuel tanks mounted on swept pylons and inboard faired rocket packets mounted on unswept pylons
6. Basic model with canopy and dorsal fin removed (no external stores)

Pressure distribution data were obtained for the basic model and for the model fitted with four faired rocket packets mounted on straight pylons. These tests were conducted at Mach numbers of 1.20, 1.30, and 1.70 at a Reynolds number of 2.0 million. Data were obtained through an angle-of-attack range of  $-3^\circ$  to  $+12^\circ$  at  $2^\circ$  increments for the basic model and  $4^\circ$  increments for tests of the model fitted with the rocket packets. A tabulation of the test conditions is presented in table II.

#### Reduction of Data

The test data have been reduced to standard NACA coefficient form based on the total projected wing area including the area in the region formed by extending the leading and trailing edges to the plane of symmetry (fig. 1). Factors which could affect the accuracy of these results and the corrections applied are discussed in the following paragraphs.

Angle of attack.- The determination of the actual angle of attack of the model under load required several corrections to be applied to the nominal angle. Corrections, determined from static load calibrations, were applied for the angular deflection of the sting and balance under aerodynamic load and for the angular movement due to structural clearance in the model support and balance. These corrections amounted to from 5 to 10 percent of the nominal angle, depending on the load.

Tunnel-wall interference.- Corrections to the data for the effects of the tunnel walls at subsonic speeds were made by the method of reference 4. These corrections which were added to the data were as follows:

$$\Delta\alpha = 0.377 C_L$$

$$\Delta C_D = 0.0066 C_L^2$$

The reflected bow wave did not intersect the model and so no tunnel-wall corrections were made for supersonic Mach numbers.

The effect of constriction of the flow at subsonic speeds due to the presence of the model was taken into account by the method of reference 5. This correction was calculated for conditions of zero angle of attack and was applied through the angle-of-attack range. At a Mach number of 0.90, this correction amounted to a 1-percent increase in Mach number and dynamic pressure over those values determined from calibrations of the wind tunnel without a model in place.

Support interference.- Results of a wind-tunnel test of a similar model (reference 6) show that the effects of support interference consisted primarily of a change of pressure at the base of the model. In this test the base pressure was measured and corrections were applied to adjust the pressure at the base to free-stream static pressure.<sup>1</sup> The drag values are, therefore, forebody drag coefficients.

Stream variations.- Tests were made at subsonic and supersonic speeds with the model in upright and inverted attitudes. Results of these tests showed no measurable indications of stream angle or stream curvature in the horizontal plane of the wind tunnel. Stream surveys of the Ames 6- by 6-foot supersonic wind tunnel (reference 2) show some curvature in the vertical plane of the wind tunnel, but the results of a subsequent investigation (reference 7) indicate that this curvature has little effect on the longitudinal aerodynamic characteristics of the model when pitched in the horizontal plane.

Internal duct drag.- The model was equipped with twin ducts through which air could flow. However, provisions were not made to vary the mass flow, so a study of the duct drag characteristics was not feasible in this investigation. The drag data presented herein are for the complete model; that is, the drag due to flow through the ducts has not been subtracted from the final drag coefficients.

#### Precision of Data

The accuracy of the test results, excluding stream effects, is shown by the repeatability of the data. Examination of the results showed the data to repeat with the accuracy shown in the following table:

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<sup>1</sup>The base area used in this investigation was the entire base area of the model less the duct exit area.

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Quantity	Accuracy	
	$C_L = 0$	$C_L = 0.25$
$C_D$	$\pm 0.0004$	$\pm 0.0006$
$C_L$	$\pm .0016$	$\pm .0018$
$C_m$	$\pm .0005$	$\pm .0005$
$C_l$	$\pm .0006$	$\pm .0009$
$C_p$	$\pm .005$	$\pm .005$
M	$\pm .03$	$\pm .03$
R	$\pm .03 \times 10^6$	$\pm .03 \times 10^6$
$\alpha$	$\pm .1$	$\pm .15$

The precision of the data presented herein is superior to that of the data in reference 1 because these data were obtained for a consecutive series of tests in the wind tunnel and the mounting of the model and balance was unchanged during this investigation.

## RESULTS AND DISCUSSION

Only the data pertinent to a study of the effects of external fuel tanks and rocket packets on the drag characteristics of the model are discussed in this report. All the force and moment data obtained from these tests, including lift and rolling-moment coefficients and lift-drag ratios, are presented in table III, however. In addition, experimental static pressure coefficients obtained at Mach numbers of 1.20, 1.30, and 1.70 for the basic model and for the model fitted with four rocket packets are presented in table IV. Comparison of the data from these pressure distribution tests gives an indication of the effects of the rocket-packet installation on the air loads experienced by the model.

The effects of external stores on the drag characteristics of the model are presented in this report as the increments of drag coefficient incurred by the addition of external stores. Figure 5 presents the variation of drag coefficient with lift coefficient for the basic model at Mach numbers of 0.60, 0.80, 0.90, 1.20, 1.35, 1.50, and 1.70. As previously mentioned, the drag coefficients presented in this report include the internal duct drag. The increments of drag coefficient for the various store installations investigated are shown in figure 6 as a function of Mach number for 0 and 0.25 lift coefficients. This figure shows that at subsonic speeds the drag increment resulting from the addition of four rocket packets was somewhat less when the packets were faired, but at supersonic speeds fairing the packets increased the drag. The drag increments for two fuel tanks and four rocket packets, mounted in the aft chordwise location (unswept pylons), varied from approximately 30 percent of the drag of the basic model at a Mach number of 0.60 to 50 percent at

a Mach number of 0.90. For Mach numbers of 1.20 to 1.70 the drag increment for these same external-store configurations was approximately 30 percent of the drag of the basic model. Results of tests of the model with the stores mounted in two chordwise locations showed that the change in chordwise location had no significant effect on the drag at subsonic speeds. At supersonic speeds, however, the drag increment resulting from the addition of two fuel tanks and four rocket packets was somewhat smaller for the forward chordwise location (swept pylons).

The maximum lift-drag ratios for all the configurations tested are shown in figure 7 as a function of Mach number. These data are for the unbalanced model.

Results of this investigation show that the addition of external stores could appreciably affect the trim drag of the model. This effect is illustrated in figure 8 which shows the variation of pitching-moment coefficient with lift coefficient for the basic model and for the model fitted with two external fuel tanks and four rocket packets. The magnitude of the pitching-moment coefficient at zero lift for the basic model was quite small at all Mach numbers, but the model fitted with external stores showed a significant negative pitching moment at subsonic speeds and a positive pitching moment at supersonic speeds. These pitching moments, associated with the installation of external stores on the model, significantly influence the deflection of the longitudinal control surface required for a specific flight condition. Thus it should be noted that the drag coefficients presented for this investigation are for the unbalanced model and that the total drag for the model balanced with a control device will include an additional drag increment or decrement due to the change in control setting required to counteract the aerodynamic influence of the external store. Pitching-moment characteristics are shown for the model fitted with two fuel tanks and four rocket packets because they exhibit the most pronounced effects of external stores of all the configurations investigated.

### CONCLUSIONS

The following conclusions are based on a wind-tunnel investigation of the effects of external fuel tanks and externally mounted rocket packets on the drag characteristics of a model of a tailless fighter airplane:

1. The drag increase resulting from the addition of two external fuel tanks and four faired rocket packets varied from 30 percent of the drag of the basic model at 0.60 Mach number to 50 percent of the drag of the basic model at 0.90 Mach number. At Mach numbers of 1.20 to 1.70, this drag increment was approximately 30 percent of the drag of the basic model.

2. The drag coefficient, at subsonic speeds, for the model fitted with four faired rocket packets was smaller than with four open rocket packets. At supersonic speeds the four faired packets produced greater drag increments than the open packets.

3. The drag coefficients for the model fitted with two fuel tanks and four faired rocket packets were somewhat less, at supersonic speeds, with the outboard rocket packets and fuel tanks in a forward chordwise location. At subsonic speeds the chordwise location caused no significant effect on the drag characteristics.

Ames Aeronautical Laboratory  
National Advisory Committee for Aeronautics  
Moffett Field, Calif.

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TABLE III.- CONTINUED  
(c) Tests 24 through 38

Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$	Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$	Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$
24	-0.13	-0.036	0.0480	0.015	-0.0002	-	29	-0.60	-0.036	0.0471	-0.008	-0.0010	-	34	0.56	0.022	0.0470	0.002	-0.0007	0.47
	-2.19	-0.134	0.0476	0.033	-0.0002	-		-2.87	-0.123	0.0490	-0.005	-0.0012	-		2.17	0.088	0.0490	-0.013	-0.0010	1.80
	-0.75	0.012	0.0409	0.006	-0.0004	0.29		0.38	0.008	0.041	-0.009	-0.0010	0.77		4.88	0.176	0.0776	-0.034	-0.0014	3.05
	2.20	0.101	0.0427	-0.009	-0.0004	2.36		2.19	0.101	0.0422	-0.012	-0.0009	6.65		6.39	0.257	0.0720	-0.077	-0.0015	3.68
	4.37	0.330	0.0537	-0.034	-0.0009	4.30		4.10	0.219	0.0218	-0.018	-0.0006	10.02		8.70	0.354	0.0934	-0.079	-0.0019	3.79
	6.74	0.365	0.0774	-0.065	-0.0021	4.86		6.61	0.350	0.0406	-0.028	-0.0006	8.62		8.70	0.994	-	-	-	-
25	8.69	0.493	0.1068	-0.095	-0.0006	4.62	30	8.83	0.487	0.0748	-0.043	0.012	6.72	35	0.56	-0.069	0.0437	-0.008	-0.0011	-
	-0.10	-0.022	0.0423	0.012	-0.0011	-		-2.65	-0.048	0.0487	-0.009	-0.0011	-		2.17	0.088	0.0490	-0.013	-0.0010	1.80
	-2.15	-0.112	0.0476	0.031	-0.0010	-		0.38	0.004	0.0470	-0.011	-0.0011	0.77		4.88	0.176	0.0776	-0.034	-0.0014	3.05
	2.20	0.106	0.0442	-0.015	-0.0012	2.40		2.20	0.106	0.0473	-0.015	-0.0010	6.11		6.39	0.257	0.0720	-0.077	-0.0015	3.68
	4.37	0.284	0.0773	-0.041	-0.0015	4.04		4.16	0.243	0.0294	-0.023	-0.0008	9.56		8.70	0.994	-	-	-	-
	6.49	0.340	0.0773	-0.069	-0.0009	4.50		6.73	0.409	0.0505	-0.046	-0.0004	8.10		8.65	0.339	0.0325	-0.023	-0.0005	9.56
26	8.64	0.451	0.1038	-0.094	-0.0001	4.35	31	8.82	0.411	0.0712	-0.075	-	5.90	36	0.60	-0.036	0.0448	-0.010	-0.0009	-
	-0.10	-0.017	0.0423	0.011	-0.0016	-		-2.14	-0.048	0.0466	0.019	0	-		2.28	-0.036	0.0448	-0.010	-0.0009	-
	-2.15	-0.101	0.0472	0.030	-0.0015	-		0.19	-0.145	0.0733	0.039	0	-		1.05	0.099	0.042	-0.011	-0.0011	2.67
	2.20	0.092	0.0420	-0.002	-0.0019	2.2		2.19	-	0.0421	0.010	-0.0004	1.98		8.19	0.102	0.042	-0.012	-0.0010	6.61
	4.32	0.203	0.0549	-0.041	-0.0018	3.70		4.36	0.221	0.0722	-0.006	-0.0006	4.01		4.10	0.221	0.0221	-0.019	-0.0006	9.99
	6.45	0.309	0.0789	-0.067	-0.0016	4.84		6.72	0.378	0.0760	-0.065	0	4.71		6.62	0.322	0.0410	-0.068	-0.0004	8.78
27	8.78	0.410	0.0984	-0.092	-0.0013	4.17	32	8.67	0.487	0.1066	-0.096	-	4.57	37	0.60	-0.046	0.0488	-0.012	-0.0010	-
	-0.10	-0.014	0.0435	0.008	-0.0007	-		-2.04	-0.07	0.0468	0.018	-0.0011	-		2.25	-0.046	0.0488	-0.012	-0.0010	-
	-2.13	-0.087	0.0471	0.024	-0.0003	-		0.19	-0.115	0.0722	0.036	-0.0011	-		1.05	0.099	0.042	-0.011	-0.0011	2.67
	2.20	0.088	0.0430	-0.003	-0.0013	1.8		2.20	0.100	0.0476	-0.010	-0.0016	2.10		8.19	0.102	0.042	-0.012	-0.0010	6.61
	4.27	0.174	0.0542	-0.016	-0.0013	1.87		4.37	0.217	0.0772	-0.038	-0.0014	3.76		4.16	0.221	0.0221	-0.019	-0.0006	9.99
	6.72	0.263	0.0694	-0.060	-0.0019	3.82		6.49	0.337	0.0772	-0.067	-0.0009	4.94		6.73	0.409	0.0204	-0.044	-0.0008	8.78
28	8.49	0.354	0.0912	-0.082	-0.0021	3.88	33	8.65	0.414	0.1045	-0.093	-0.0002	4.25	38	0.60	-0.047	0.0461	-0.016	-0.0003	-
	-0.10	-0.031	0.0434	0.006	-0.0011	-		-2.39	-0.020	0.0466	0.016	-0.0018	-		2.10	-0.047	0.0461	-0.016	-0.0003	-
	-2.20	-0.110	0.0460	-0.004	-0.0013	-		0.19	-0.101	0.0713	0.033	-0.0015	-		1.05	0.099	0.042	-0.011	-0.0011	2.67
	2.20	0.092	0.0432	-0.007	-0.0011	1.8		2.20	0.098	0.0481	-0.012	-0.0020	2.04		8.19	0.102	0.042	-0.012	-0.0010	6.61
	4.27	0.165	0.0542	-0.010	-0.0008	6.49		4.33	0.202	0.0771	-0.038	-0.0015	3.50		4.16	0.221	0.0221	-0.019	-0.0006	9.99
	6.46	0.317	0.0829	-0.063	-0.0002	9.62		6.46	0.304	0.0747	-0.064	-0.0015	4.07		6.62	0.322	0.0410	-0.068	-0.0004	8.78

TABLE III.- CONCLUDED  
(d) Tests 39 through 43

Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_I$	$L/D$
39	-0.40	-0.085	0.0460	0.015	-0.0012	---
	-2.16	-0.115	0.011	0.033	-0.003	---
	.57	.080	.0454	.006	-.0014	0.44
	1.11	.044	.0456	.001	-.0015	.96
	2.20	.101	.0475	-.012	-.0018	2.12
	4.35	.219	.0581	-.039	-.0015	3.77
	6.49	.337	.0774	-.067	-.0009	4.36
	8.63	.445	.1048	-.093	0	4.24
	-.39	-.018	.0457	.013	-.0017	---
	-2.14	-.102	.0498	.030	-.0014	---
40	.57	.084	.0454	.004	-.0020	.53
	1.11	.044	.0456	-.001	-.0021	.96
	2.20	.099	.0478	-.014	-.0020	2.07
	4.33	.205	.0778	-.039	-.0018	3.57
	6.46	.309	.0792	-.065	-.0015	4.11
	8.58	.408	.1001	-.089	-.0011	4.08
	-.39	-.018	.0457	.013	-.0017	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
41	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
	-.39	-.011	.0462	.007	-.0008	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
42	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
	-.39	-.011	.0462	.007	-.0008	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
43	17.21	0.884	0.2433	-0.069	0.0005	3.39
	19.29	.875	.2304	-.076	.0007	2.93
	21.33	.901	.3499	-.086	-.0005	2.58
	-.56	-.024	.0110	-.002	-.0011	---
	-1.11	-.051	.0115	-.002	-.0012	---
	-3.32	-.163	.0165	-.004	-.0015	---
	-6.64	-.339	.0430	-.022	-.0015	---
	.53	.080	.0110	-.005	-.0011	1.82
	1.09	.051	.0113	-.006	-.0011	4.51
	2.21	.108	.0130	-.010	-.0010	8.28
44	4.40	.223	.0805	-.017	-.0008	10.90
	6.61	.351	.0398	-.023	.0005	8.22
	8.82	.486	.0723	-.045	.0005	6.72
	11.00	.593	.1138	-.056	.0011	5.21
	13.15	.676	.1590	-.062	.0023	4.25
	15.26	.737	.2038	-.069	.0005	3.62
	17.36	.797	.2566	-.078	.0008	3.10
	-.57	-.029	.0109	-.002	-.0013	---
	-1.14	-.058	.0114	0	-.0013	---
	-3.39	-.189	.0185	.010	-.0015	---
45	.53	.019	.0108	-.004	-.0011	1.76
	1.11	.053	.011	-.006	-.0011	4.77
	2.29	.117	.0232	-.011	-.0010	8.88
	4.48	.249	.0230	-.023	-.0008	10.83
	6.73	.412	.0508	-.050	-.0006	8.12
	8.92	.510	.0888	-.075	-.0005	6.16
	-.54	-.024	.0321	.004	-.0001	---
	-3.28	-.182	.0443	.078	.0004	---
	-6.52	-.383	.0743	.078	.0007	---
	.54	.021	.0348	-.004	.0004	.60
46	1.09	.053	.0356	-.009	.0005	1.51
	2.19	.113	.0776	-.020	.0023	3.01
	4.35	.238	.0490	-.047	.0027	4.86
	6.51	.372	.0707	-.077	-.0001	5.29
	8.66	.499	.1017	-.106	.0010	4.51
	10.81	.613	.1405	-.131	.0017	4.36
	12.96	.696	.1799	-.146	.0025	3.87
	-.54	-.022	0.0375	0.003	-0.0009	---
	-1.09	-.051	.0363	.009	-.0009	---
	-3.23	-.162	.0442	.033	-.0006	---
47	-6.47	-.340	.0718	.074	-.0002	---
	.52	.017	.0332	-.004	-.0010	0.48
	1.06	.046	.0353	-.010	-.0011	1.30
	2.17	.102	.0374	-.022	-.0012	2.73
	4.31	.214	.0480	-.047	-.0010	4.46
	6.45	.330	.0671	-.075	-.0006	4.92
	8.59	.442	.0946	-.102	-.0004	4.67
	10.73	.541	.1248	-.127	.0009	3.28
	12.86	.644	.1716	-.149	.0013	3.75
	-.54	-.022	.0345	.004	-.0015	---
48	-1.09	-.049	.0332	.009	-.0015	---
	-3.24	-.152	.0434	.032	-.0010	---
	-6.44	-.310	.0689	.070	-.0006	---
	.52	.014	.0344	-.004	-.0016	.41
	1.07	.040	.0346	-.010	-.0017	1.16
	2.16	.092	.0368	-.021	-.0019	2.50
	4.28	.194	.0466	-.045	-.0018	4.17
	6.41	.293	.0638	-.070	-.0015	4.67
	8.54	.397	.0883	-.095	-.0012	4.50
	10.66	.491	.1198	-.118	-.0008	4.11
49	12.78	.580	.1568	-.139	-.0008	3.70
	-.54	-.019	.0346	.001	-.0008	---
	-1.08	-.042	.0353	.005	-.0006	---
	-3.22	-.134	.0425	.063	-.0002	---
	-6.39	-.271	.0636	.079	.0008	---
	.40	.012	.0342	-.006	-.0010	.55
	.94	.037	.0345	-.011	-.0012	1.01
	2.13	.082	.0365	-.022	-.0012	2.24
	4.24	.172	.0454	-.043	-.0015	3.79
	6.36	.261	.0602	-.064	-.0017	4.33
50	8.47	.348	.0819	-.095	-.0016	4.25
	10.58	.430	.1089	-.105	-.0016	3.95
	12.69	.508	.1414	-.124	-.0017	3.59
	-.54	-.019	.0346	.001	-.0008	---
	-1.08	-.042	.0353	.005	-.0006	---
	-3.22	-.134	.0425	.063	-.0002	---
	-6.39	-.271	.0636	.079	.0008	---
	.40	.012	.0342	-.006	-.0010	.55
	.94	.037	.0345	-.011	-.0012	1.01
	2.13	.082	.0365	-.022	-.0012	2.24

NACA

TABLE IV.- EXPERIMENTAL PRESSURE COEFFICIENTS,  $C_p$   
(a) Basic model,  $M = 1.2$

Orifice No.	Angle of attack										Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°		-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
0	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	34	-0.103	-0.076	-0.061	-0.062	-0.005	0.041	0.109	0.165	0.222	0.285
1	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	35	-0.115	-0.074	-0.062	-0.030	-0.003	0.038	0.101	0.164	0.222	0.290
2	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	36	-0.126	-0.104	-0.085	-0.053	-0.032	0.018	0.074	0.138	0.197	0.257
3	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	37	-0.141	-0.117	-0.102	-0.069	-0.052	-0.003	0.046	0.097	0.157	0.218
4	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	38	-0.156	-0.128	-0.103	-0.072	-0.057	0.004	0.051	0.101	0.161	0.221
5	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	39	-0.171	-0.141	-0.113	-0.084	-0.069	0.004	0.051	0.101	0.161	0.221
6	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	40	-0.186	-0.154	-0.124	-0.094	-0.079	0.004	0.051	0.101	0.161	0.221
7	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	41	-0.201	-0.167	-0.136	-0.106	-0.091	0.004	0.051	0.101	0.161	0.221
8	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	42	-0.216	-0.181	-0.149	-0.119	-0.104	0.004	0.051	0.101	0.161	0.221
9	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	43	-0.231	-0.195	-0.163	-0.133	-0.118	0.004	0.051	0.101	0.161	0.221
10	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	44	-0.246	-0.209	-0.177	-0.147	-0.132	0.004	0.051	0.101	0.161	0.221
11	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	45	-0.261	-0.224	-0.192	-0.162	-0.147	0.004	0.051	0.101	0.161	0.221
12	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	46	-0.276	-0.239	-0.207	-0.177	-0.162	0.004	0.051	0.101	0.161	0.221
13	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	47	-0.291	-0.254	-0.222	-0.192	-0.177	0.004	0.051	0.101	0.161	0.221
14	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	48	-0.306	-0.269	-0.237	-0.207	-0.192	0.004	0.051	0.101	0.161	0.221
15	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	49	-0.321	-0.284	-0.252	-0.222	-0.207	0.004	0.051	0.101	0.161	0.221
16	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	50	-0.336	-0.299	-0.267	-0.237	-0.222	0.004	0.051	0.101	0.161	0.221
17	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	51	-0.351	-0.314	-0.282	-0.252	-0.237	0.004	0.051	0.101	0.161	0.221
18	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	52	-0.366	-0.329	-0.297	-0.267	-0.252	0.004	0.051	0.101	0.161	0.221
19	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	53	-0.381	-0.344	-0.312	-0.282	-0.267	0.004	0.051	0.101	0.161	0.221
20	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	54	-0.396	-0.359	-0.327	-0.297	-0.282	0.004	0.051	0.101	0.161	0.221
21	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	55	-0.411	-0.374	-0.342	-0.312	-0.297	0.004	0.051	0.101	0.161	0.221
22	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	56	-0.426	-0.389	-0.357	-0.327	-0.312	0.004	0.051	0.101	0.161	0.221
23	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	57	-0.441	-0.404	-0.372	-0.342	-0.327	0.004	0.051	0.101	0.161	0.221
24	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	58	-0.456	-0.419	-0.387	-0.357	-0.342	0.004	0.051	0.101	0.161	0.221
25	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	59	-0.471	-0.434	-0.402	-0.372	-0.357	0.004	0.051	0.101	0.161	0.221
26	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	60	-0.486	-0.449	-0.417	-0.387	-0.372	0.004	0.051	0.101	0.161	0.221
27	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	61	-0.501	-0.464	-0.432	-0.402	-0.387	0.004	0.051	0.101	0.161	0.221
28	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	62	-0.516	-0.479	-0.447	-0.417	-0.402	0.004	0.051	0.101	0.161	0.221
29	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	63	-0.531	-0.494	-0.462	-0.432	-0.417	0.004	0.051	0.101	0.161	0.221
30	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	64	-0.546	-0.509	-0.477	-0.447	-0.432	0.004	0.051	0.101	0.161	0.221
31	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	65	-0.561	-0.524	-0.492	-0.462	-0.447	0.004	0.051	0.101	0.161	0.221
32	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	66	-0.576	-0.539	-0.507	-0.477	-0.462	0.004	0.051	0.101	0.161	0.221
33	1.354	1.577	1.396	1.368	1.399	1.384	1.392	1.392	1.376	1.372	67	-0.591	-0.554	-0.522	-0.492	-0.477	0.004	0.051	0.101	0.161	0.221

Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
67	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
68	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
69	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
70	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
71	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
72	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
73	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
74	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
75	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
76	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
77	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
78	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
79	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
80	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
81	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
82	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
83	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
84	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
85	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
86	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
87	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
88	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
89	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
90	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
91	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
92	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
93	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
94	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
95	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
96	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
97	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
98	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451



TABLE IV.- CONTINUED  
(b) Basic model,  $M = 1.3$

Orifice No.	Angle of attack										Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°		-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
0	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	34	-0.104	-0.091	-0.068	-0.046	-0.021	0.000	0.078	0.156	0.200	0.248
1	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	34A	-0.064	-0.059	-0.038	-0.011	-0.014	0.076	0.108	0.164	0.217	0.277
2	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	35	-0.119	-0.077	-0.087	-0.066	-0.038	0	0.049	0.096	0.153	0.203
3	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	36	-0.144	-0.131	-0.110	-0.088	-0.060	-0.030	0.017	0.066	0.113	0.169
4	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	37	-0.208	-0.215	-0.206	-0.188	-0.160	-0.126	-0.088	-0.043	0.001	0.039
5	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	38	-0.177	-0.135	-0.131	-0.100	-0.069	-0.039	-0.007	-0.027	-0.025	-0.190
6	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	39	-0.141	-0.078	-0.021	-0.074	-0.128	-0.230	-0.322	-0.403	-0.469	-0.533
7	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	40	-0.035	-0.087	-0.128	-0.154	-0.169	-0.189	-0.204	-0.213	-0.218	-0.223
8	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	41	-0.031	-0.008	-0.029	-0.107	-0.159	-0.200	-0.230	-0.241	-0.248	-0.256
9	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	42	-0.029	-0.006	-0.026	-0.084	-0.129	-0.167	-0.194	-0.213	-0.223	-0.228
10	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	43	-0.007	-0.023	-0.054	-0.080	-0.101	-0.110	-0.114	-0.116	-0.118	-0.120
11	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	44	-0.060	-0.089	-0.114	-0.141	-0.160	-0.176	-0.187	-0.194	-0.197	-0.200
12	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	45	-0.080	-0.100	-0.123	-0.141	-0.160	-0.176	-0.187	-0.194	-0.197	-0.200
13	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	46	-0.048	-0.073	-0.103	-0.139	-0.182	-0.221	-0.256	-0.284	-0.306	-0.326
14	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	47	-0.044	-0.069	-0.100	-0.136	-0.178	-0.217	-0.252	-0.280	-0.302	-0.322
15	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	48	-0.054	-0.080	-0.108	-0.146	-0.186	-0.221	-0.250	-0.273	-0.291	-0.309
16	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	49	-0.048	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
17	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	50	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
18	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	51	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
19	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	52	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
20	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	53	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
21	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	54	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
22	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	55	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
23	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	56	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
24	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	57	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
25	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	58	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
26	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	59	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
27	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	60	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
28	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	61	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
29	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	62	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
30	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	63	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
31	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	64	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
32	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	65	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322
33	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	66	-0.044	-0.083	-0.120	-0.159	-0.200	-0.235	-0.264	-0.287	-0.305	-0.322

Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
67	-0.098	-0.129	-0.151	-0.163	-0.178	-0.207	-0.236	-0.266	-0.296	-0.315
68	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
69	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
70	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
71	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
72	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
73	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
74	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
75	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
76	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
77	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
78	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
79	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
80	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
81	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
82	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
83	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
84	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
85	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
86	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
87	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
88	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
89	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
90	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
91	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
92	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
93	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
94	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
95	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
96	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
97	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256
98	-0.078	-0.098	-0.111	-0.121	-0.136	-0.159	-0.184	-0.209	-0.234	-0.256

NACA

TABLE III.- CONTINUED  
(c) Tests 24 through 38

Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$	Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$	Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_i$	$l/d$
24	-0.13	-0.036	0.0480	0.015	-0.0002	-	29	-0.60	-0.036	0.0471	-0.008	-0.0010	-	34	0.56	0.022	0.0470	0.002	-0.0007	0.47
	-2.19	-0.134	0.0476	0.033	-0.0002	-		-2.87	-0.123	0.0490	-0.005	-0.0012	-		2.17	0.088	0.0490	-0.013	-0.0010	1.80
	-0.75	0.012	0.0409	0.006	-0.0004	0.29		0.38	0.008	0.041	-0.009	-0.0010	0.57		4.88	0.176	0.0776	-0.034	-0.0014	3.05
	2.20	0.101	0.0427	-0.009	-0.0004	2.36		2.19	0.101	0.0422	-0.012	-0.0009	6.65		6.39	0.257	0.0720	-0.077	-0.0015	3.68
	4.37	0.330	0.0537	-0.034	-0.0007	4.30		4.10	0.219	0.0218	-0.018	-0.0006	10.02		8.70	0.354	0.0934	-0.079	-0.0019	3.79
25	6.74	0.365	0.0774	-0.065	-0.001	4.86	30	6.61	0.350	0.0406	-0.028	-0.0006	8.62	35	0.56	0.022	0.0437	0.008	-0.0013	-
	8.69	0.493	0.068	-0.095	-0.0006	4.62		8.83	0.487	0.0748	-0.043	-0.0012	6.72		-2.21	-0.089	0.0462	-0.008	-0.0013	-
	-0.10	-0.022	0.0423	0.012	-0.0011	-		-0.65	-0.048	0.0487	-0.009	-0.0011	-		0.39	0.011	0.0432	-0.009	-0.0011	0.83
	-2.15	-0.112	0.0476	0.031	-0.0010	-		2.19	0.004	0.0470	-0.011	-0.0011	0.23		2.15	0.099	0.0436	-0.011	-0.0010	6.42
	0.75	0.022	0.0418	0.003	-0.0012	2.3		4.48	0.106	0.0473	-0.015	-0.0010	6.11		4.32	0.203	0.0822	-0.015	-0.0005	9.56
26	2.20	0.106	0.0442	-0.015	-0.0015	2.10	31	4.16	0.243	0.0294	-0.023	-0.0008	9.56	36	6.48	0.320	0.0325	-0.023	-0.0005	9.56
	4.37	0.224	0.0777	-0.041	-0.0015	4.04		6.73	0.409	0.0505	-0.046	-0.0004	8.10		8.65	0.439	0.0549	-0.033	-0.001	8.00
	6.49	0.340	0.0777	-0.069	-0.0009	4.20		8.82	0.511	0.0712	-0.075	-	5.90		-0.60	-0.036	0.0448	-0.010	-0.0009	-
	8.64	0.451	0.1038	-0.094	-0.0001	4.35		-0.14	-0.048	0.0466	0.019	0	-		-2.28	-0.124	0.0494	-0.008	-0.0010	-
	-0.10	-0.017	0.0423	0.011	-0.0016	-		-2.19	-0.145	0.0733	0.039	0	-		0.38	0.009	0.0442	-0.011	-0.0011	0.63
27	-2.15	-0.101	0.0472	0.030	-0.0015	-	32	2.19	0.090	0.0472	-0.006	-0.0004	1.98	37	1.05	0.038	0.0442	-0.012	-0.0010	2.67
	0.75	0.022	0.0420	0.002	-0.0019	2.2		4.16	0.221	0.0722	-0.033	-0.0006	4.01		2.19	0.102	0.0471	-0.019	-0.0008	6.61
	2.16	0.085	0.0472	-0.016	-0.0013	2.82		4.35	0.221	0.0722	-0.033	-0.0006	4.01		4.10	0.221	0.0471	-0.019	-0.0008	9.99
	4.27	0.203	0.0549	-0.041	-0.0016	3.70		6.22	0.378	0.0760	-0.065	0	4.71		6.62	0.322	0.0410	-0.038	-0.0004	8.58
	6.45	0.309	0.0789	-0.067	-0.0016	4.84		8.67	0.487	0.1066	-0.096	-	4.57		8.85	0.490	0.0720	-0.040	-0.0005	6.81
28	8.28	0.410	0.0984	-0.092	-0.0013	4.17	33	-0.10	-0.027	0.0468	0.018	-0.0011	-	38	-0.4	-0.046	0.0488	-0.012	-0.0010	-
	-0.10	-0.014	0.0495	0.008	-0.0007	-		-2.04	-0.115	0.0522	0.036	-0.0011	-		-2.35	-0.149	0.0650	-0.006	-0.0013	-
	-2.13	-0.087	0.0471	0.024	-0.0003	-		2.20	0.100	0.0476	-0.010	-0.0016	2.10		0.48	0.006	0.0471	-0.013	-0.0010	3.5
	0.75	0.022	0.0430	0	-0.0019	1.2		4.16	0.217	0.0772	-0.038	-0.0014	3.76		2.21	0.108	0.0477	-0.015	-0.0011	2.33
	2.16	0.085	0.0472	-0.016	-0.0013	1.87		4.35	0.217	0.0772	-0.038	-0.0014	3.76		4.16	0.107	0.0477	-0.015	-0.0010	6.16

TABLE III.- CONCLUDED  
(d) Tests 39 through 43

Test No.	$\alpha$	$C_L$	$C_D$	$C_M$	$C_I$	$L/D$
39	-0.40	-0.085	0.0460	0.015	-0.0012	---
	-2.16	-0.115	0.011	0.033	-0.003	---
	.57	.080	.0454	.006	-.0014	0.44
	1.11	.044	.0456	.001	-.0015	.96
	2.20	.101	.0475	-.012	-.0018	2.12
	4.35	.219	.0581	-.039	-.0015	3.77
	6.49	.337	.0774	-.067	-.0009	4.36
	8.63	.445	.1048	-.093	0	4.24
	-.39	-.018	.0457	.013	-.0017	---
	-2.14	-.102	.0498	.030	-.0014	---
40	.57	.084	.0454	.004	-.0020	.53
	1.11	.044	.0456	-.001	-.0021	.96
	2.20	.099	.0478	-.014	-.0020	2.07
	4.33	.205	.0778	-.039	-.0018	3.57
	6.46	.309	.0792	-.065	-.0015	4.11
	8.58	.408	.1001	-.089	-.0011	4.08
	-.39	-.018	.0457	.013	-.0017	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
41	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
	-.39	-.011	.0462	.007	-.0008	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
42	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
	-.39	-.011	.0462	.007	-.0008	---
	-2.13	-.089	.0456	.024	-.0003	---
	.57	.080	.0460	0	-.0009	.44
	1.09	.043	.0460	-.005	-.0010	.93
	2.17	.090	.0482	-.016	-.0012	1.87
	4.28	.179	.0770	-.036	-.0015	3.14
	6.40	.268	.0719	-.058	-.0017	3.72
	8.51	.358	.0937	-.080	-.0018	3.82
43	17.21	0.884	0.2433	-0.069	0.0005	3.39
	19.29	.875	.2304	-.076	.0007	2.93
	21.33	.901	.3499	-.086	-.0005	2.58
	-.56	-.024	.0110	-.002	-.0011	---
	-1.11	-.051	.0115	-.002	-.0012	---
	-3.32	-.163	.0165	-.004	-.0015	---
	-6.64	-.339	.0430	-.022	-.0015	---
	.53	.080	.0110	-.005	-.0011	1.82
	1.09	.051	.0113	-.006	-.0011	4.51
	2.21	.108	.0130	-.010	-.0010	8.28
44	4.40	.223	.0805	-.017	-.0008	10.90
	6.61	.351	.0398	-.023	.0005	8.22
	8.82	.486	.0723	-.045	.0005	6.72
	11.00	.593	.1138	-.056	.0011	5.21
	13.15	.676	.1590	-.062	.0023	4.25
	15.26	.737	.2038	-.069	.0005	3.62
	17.36	.797	.2566	-.078	.0008	3.10
	-.57	-.029	.0109	-.002	-.0013	---
	-1.14	-.058	.0114	0	-.0013	---
	-3.39	-.189	.0185	.010	-.0015	---
45	.53	.019	.0108	-.004	-.0011	1.76
	1.11	.053	.011	-.006	-.0011	4.77
	2.29	.117	.0232	-.011	-.0010	8.88
	4.48	.249	.0230	-.023	-.0008	10.83
	6.73	.412	.0508	-.050	-.0006	8.12
	8.92	.510	.0888	-.075	-.0002	6.16
	-.54	-.024	.0321	.004	-.0001	---
	-3.28	-.182	.0443	.078	.0004	---
	-6.52	-.383	.0743	.078	.0007	---
	.54	.021	.0348	-.004	.0004	.60
46	1.09	.053	.0356	-.009	.0005	1.51
	2.19	.113	.0776	-.020	.0023	3.01
	4.35	.238	.0490	-.047	.0027	4.86
	6.51	.372	.0707	-.077	-.0001	5.29
	8.66	.499	.1017	-.106	.0010	4.51
	10.81	.613	.1405	-.131	.0017	4.36
	12.96	.696	.1799	-.146	.0025	3.87
	-.54	-.022	0.0355	0.003	-0.0009	---
	-1.09	-.051	.0363	.009	-.0009	---
	-3.23	-.162	.0442	.033	-.0006	---
47	-6.47	-.340	.0718	.074	-.0002	---
	.52	.017	.0352	-.004	-.0010	0.48
	1.06	.046	.0353	-.010	-.0011	1.30
	2.17	.102	.0374	-.022	-.0012	2.73
	4.31	.214	.0480	-.047	-.0010	4.46
	6.45	.330	.0671	-.075	-.0006	4.92
	8.59	.442	.0946	-.102	-.0004	4.67
	10.73	.541	.1248	-.127	.0009	3.28
	12.86	.644	.1716	-.149	.0013	3.75
	-.54	-.022	.0345	.004	-.0015	---
48	-1.09	-.049	.0352	.009	-.0015	---
	-3.24	-.152	.0434	.032	-.0010	---
	-6.44	-.310	.0689	.070	-.0006	---
	.52	.014	.0344	-.004	-.0016	.41
	1.07	.040	.0346	-.010	-.0017	1.16
	2.16	.092	.0368	-.021	-.0019	2.50
	4.28	.194	.0466	-.045	-.0018	4.17
	6.41	.293	.0638	-.070	-.0015	4.67
	8.54	.397	.0883	-.095	-.0012	4.50
	10.66	.491	.1198	-.118	-.0008	4.11
49	12.78	.580	.1568	-.139	-.0008	3.70
	-.54	-.019	.0346	.001	-.0008	---
	-1.08	-.042	.0353	.006	-.0006	---
	-3.22	-.134	.0425	.063	-.0002	---
	-6.39	-.271	.0636	.079	.0008	---
	.54	.012	.0342	-.006	-.0010	.55
	1.13	.037	.0345	-.011	-.0012	1.24
	2.13	.082	.0365	-.022	-.0015	2.24
	4.24	.172	.0454	-.043	-.0015	3.79
	6.36	.261	.0602	-.064	-.0017	4.33
50	8.47	.348	.0819	-.095	-.0016	4.25
	10.58	.430	.1089	-.105	-.0016	3.95
	12.69	.508	.1414	-.124	-.0017	3.59
	-.54	-.022	0.0355	0.003	-0.0009	---
	-1.09	-.051	.0363	.009	-.0009	---
	-3.23	-.162	.0442	.033	-.0006	---
	-6.47	-.340	.0718	.074	-.0002	---
	.52	.017	.0352	-.004	-.0010	0.48
	1.06	.046	.0353	-.010	-.0011	1.30
	2.17	.102	.0374	-.022	-.0012	2.73

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TABLE IV.- EXPERIMENTAL PRESSURE COEFFICIENTS,  $C_p$   
(a) Basic model,  $M = 1.2$

Orifice No.	Angle of attack										Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°		-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
0	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	34	-0.103	-0.076	-0.061	-0.062	-0.005	0.041	0.109	0.165	0.222	0.285
1	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	35	-0.115	-0.074	-0.062	-0.030	-0.003	0.038	0.101	0.164	0.223	0.290
2	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	36	-0.126	-0.104	-0.085	-0.053	-0.032	0.018	0.074	0.138	0.187	0.237
3	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	37	-0.141	-0.117	-0.102	-0.069	-0.052	-0.003	0.046	0.097	0.135	0.188
4	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	38	-0.156	-0.128	-0.103	-0.072	-0.057	0.004	0.051	0.097	0.135	0.188
5	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	39	-0.171	-0.141	-0.113	-0.084	-0.069	0.004	0.051	0.097	0.135	0.188
6	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	40	-0.186	-0.154	-0.126	-0.097	-0.082	0.004	0.051	0.097	0.135	0.188
7	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	41	-0.201	-0.168	-0.139	-0.110	-0.095	0.004	0.051	0.097	0.135	0.188
8	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	42	-0.216	-0.183	-0.154	-0.125	-0.110	0.004	0.051	0.097	0.135	0.188
9	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	43	-0.231	-0.198	-0.169	-0.140	-0.125	0.004	0.051	0.097	0.135	0.188
10	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	44	-0.246	-0.213	-0.184	-0.155	-0.140	0.004	0.051	0.097	0.135	0.188
11	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	45	-0.261	-0.228	-0.199	-0.170	-0.155	0.004	0.051	0.097	0.135	0.188
12	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	46	-0.276	-0.243	-0.214	-0.185	-0.170	0.004	0.051	0.097	0.135	0.188
13	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	47	-0.291	-0.258	-0.229	-0.200	-0.185	0.004	0.051	0.097	0.135	0.188
14	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	48	-0.306	-0.273	-0.244	-0.215	-0.200	0.004	0.051	0.097	0.135	0.188
15	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	49	-0.321	-0.288	-0.259	-0.230	-0.215	0.004	0.051	0.097	0.135	0.188
16	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	50	-0.336	-0.303	-0.274	-0.245	-0.230	0.004	0.051	0.097	0.135	0.188
17	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	51	-0.351	-0.318	-0.289	-0.260	-0.245	0.004	0.051	0.097	0.135	0.188
18	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	52	-0.366	-0.333	-0.304	-0.275	-0.260	0.004	0.051	0.097	0.135	0.188
19	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	53	-0.381	-0.348	-0.319	-0.290	-0.275	0.004	0.051	0.097	0.135	0.188
20	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	54	-0.396	-0.363	-0.334	-0.305	-0.290	0.004	0.051	0.097	0.135	0.188
21	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	55	-0.411	-0.378	-0.349	-0.320	-0.305	0.004	0.051	0.097	0.135	0.188
22	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	56	-0.426	-0.393	-0.364	-0.335	-0.320	0.004	0.051	0.097	0.135	0.188
23	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	57	-0.441	-0.408	-0.379	-0.350	-0.335	0.004	0.051	0.097	0.135	0.188
24	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	58	-0.456	-0.423	-0.394	-0.365	-0.350	0.004	0.051	0.097	0.135	0.188
25	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	59	-0.471	-0.438	-0.409	-0.380	-0.365	0.004	0.051	0.097	0.135	0.188
26	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	60	-0.486	-0.453	-0.424	-0.395	-0.380	0.004	0.051	0.097	0.135	0.188
27	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	61	-0.501	-0.468	-0.439	-0.410	-0.395	0.004	0.051	0.097	0.135	0.188
28	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	62	-0.516	-0.483	-0.454	-0.425	-0.410	0.004	0.051	0.097	0.135	0.188
29	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	63	-0.531	-0.498	-0.469	-0.440	-0.425	0.004	0.051	0.097	0.135	0.188
30	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	64	-0.546	-0.513	-0.484	-0.455	-0.440	0.004	0.051	0.097	0.135	0.188
31	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	65	-0.561	-0.528	-0.499	-0.470	-0.455	0.004	0.051	0.097	0.135	0.188
32	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	66	-0.576	-0.543	-0.514	-0.485	-0.470	0.004	0.051	0.097	0.135	0.188
33	1.354	1.577	1.396	1.368	1.399	1.384	1.362	1.352	1.376	1.352	67	-0.591	-0.558	-0.529	-0.500	-0.485	0.004	0.051	0.097	0.135	0.188

Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
67	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
68	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
69	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
70	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
71	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
72	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
73	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
74	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
75	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
76	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
77	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
78	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
79	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
80	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
81	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
82	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
83	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
84	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
85	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
86	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
87	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
88	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
89	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
90	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
91	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
92	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
93	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
94	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
95	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
96	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
97	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451
98	-0.063	-0.131	-0.156	-0.164	-0.184	-0.222	-0.262	-0.320	-0.401	-0.451

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TABLE IV.- CONTINUED  
(b) Basic model,  $M = 1.3$

Orifice No.	Angle of attack										Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°		-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
0	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	34	-0.104	-0.091	-0.068	-0.046	-0.021	0.000	0.078	0.156	0.200	0.248
1	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	34A	-0.064	-0.059	-0.038	-0.011	-0.014	0.076	0.108	0.164	0.217	0.277
2	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	35	-0.119	-0.077	-0.087	-0.066	-0.038	0	0.049	0.096	0.153	0.203
3	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	36	-0.144	-0.131	-0.110	-0.088	-0.060	-0.030	0.017	0.066	0.113	0.169
4	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	37	-0.208	-0.215	-0.206	-0.188	-0.160	-0.126	-0.088	-0.043	0.001	0.039
5	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	38	-0.177	-0.135	-0.131	-0.100	-0.069	-0.039	-0.007	-0.027	-0.025	-0.190
6	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	39	-0.141	-0.078	-0.021	-0.074	-0.128	-0.230	-0.322	-0.403	-0.469	-0.533
7	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	40	-0.035	-0.087	-0.128	-0.154	-0.169	-0.189	-0.204	-0.213	-0.218	-0.223
8	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	41	-0.031	-0.008	-0.029	-0.107	-0.159	-0.200	-0.230	-0.241	-0.248	-0.256
9	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	42	-0.029	-0.006	-0.026	-0.084	-0.129	-0.167	-0.194	-0.213	-0.223	-0.228
10	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	43	-0.007	-0.023	-0.054	-0.080	-0.101	-0.110	-0.114	-0.116	-0.118	-0.120
11	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	44	-0.060	-0.089	-0.114	-0.141	-0.160	-0.176	-0.187	-0.194	-0.197	-0.200
12	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	45	-0.080	-0.100	-0.123	-0.141	-0.160	-0.176	-0.187	-0.194	-0.197	-0.200
13	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	46	-0.048	-0.073	-0.103	-0.139	-0.182	-0.221	-0.256	-0.284	-0.306	-0.326
14	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	47	-0.044	-0.069	-0.100	-0.136	-0.178	-0.217	-0.252	-0.280	-0.302	-0.319
15	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	48	-0.094	-0.080	-0.108	-0.146	-0.186	-0.221	-0.250	-0.271	-0.287	-0.299
16	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	49	-0.248	-0.163	-0.080	-0.003	-0.076	-0.164	-0.257	-0.335	-0.414	-0.475
17	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	50	-	-	-	-	-	-	-	-	-	-
18	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	51	-	-	-	-	-	-	-	-	-	-
19	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	52	-0.200	-0.171	-0.139	-0.099	-0.057	-0.001	0.066	0.139	0.216	0.293
20	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	53	-0.168	-0.130	-0.085	-0.033	-0.021	0.006	0.055	0.114	0.178	0.235
21	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	54	-0.197	-0.158	-0.100	-0.034	-0.104	-0.066	-0.017	0.032	0.087	0.143
22	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	55	-0.193	-0.150	-0.083	-0.019	-0.114	-0.064	-0.037	0.007	0.058	0.092
23	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	56	-	-	-	-	-	-	-	-	-	-
24	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	57	-0.154	-0.161	-0.131	-0.140	-0.186	-0.201	-0.089	-0.089	0.017	0.097
25	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	58	-0.193	-0.193	-0.181	-0.163	-0.138	-0.111	-0.087	-0.033	-0.014	0.054
26	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	59	-0.198	-0.097	-0.010	-0.071	-0.139	-0.241	-0.343	-0.443	-0.495	-0.533
27	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	60	-0.048	-0.015	-0.104	-0.183	-0.243	-0.313	-0.410	-0.477	-0.531	-0.579
28	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	61	-0.083	-0.030	-0.086	-0.139	-0.195	-0.268	-0.371	-0.436	-0.474	-0.507
29	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	62	-0.019	-0.068	-0.072	-0.123	-0.178	-0.250	-0.378	-0.443	-0.504	-0.552
30	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	63	-0.001	-0.036	-0.076	-0.108	-0.119	-0.165	-0.286	-0.380	-0.441	-0.486
31	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	64	-0.030	-0.087	-0.097	-0.119	-0.136	-0.174	-0.216	-0.307	-0.382	-0.440
32	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	65	-0.094	-0.116	-0.148	-0.170	-0.179	-0.215	-0.246	-0.310	-0.380	-0.443
33	1.438	1.437	1.448	1.449	1.463	1.479	1.494	1.443	1.432	1.411	66	-0.107	-0.135	-0.158	-0.178	-0.193	-0.218	-0.251	-0.296	-0.348	-0.404

Orifice No.	Angle of attack									
	-3°	-1°	0°	1°	2°	3°	4°	5°	6°	7°
67	-0.098	-0.129	-0.151	-0.163	-0.178	-0.207	-0.236	-0.266	-0.346	-0.415
68	-0.078	-0.098	-0.111	-0.131	-0.146	-0.178	-0.199	-0.234	-0.297	-0.366
69	-	-	-	-	-	-	-	-	-	-
70	-	-	-	-	-	-	-	-	-	-
71	-	-	-	-	-	-	-	-	-	-
72	-0.289	-0.290	-0.198	-0.130	-0.101	-0.083	0.068	0.196	0.233	0.310
73	-0.293	-0.217	-0.160	-0.109	-0.068	0.001	0.073	0.196	0.219	0.266
74	-	-	-	-	-	-	-	-	-	-
75	-0.201	-0.193	-0.170	-0.138	-0.118	-0.067	-0.011	0.093	0.103	0.164
76	-0.210	-0.193	-0.174	-0.136	-0.137	-0.100	-0.047	0.019	0.066	0.120
77	-0.216	-0.203	-0.188	-0.178	-0.156	-0.129	-0.076	-0.015	0.045	0.088
78	-0.175	-0.194	-0.157	-0.127	-0.108	-0.053	-0.018	0.035	0.063	0.100
79	-0.207	-0.190	-0.170	-0.164	-0.140	-0.108	-0.055	-0.009	0.087	0.070
80	-0.210	-0.196	-0.182	-0.167	-0.148	-0.119	-0.077	-0.039	-0.005	0.038
81	-0.220	-0.196	-0.190	-0.169	-0.143	-0.118	-0.077	-0.036	-0.005	0.076
82	-0.241	-0.231	-0.200	-0.189	-0.173	-0.141	-0.104	-0.061	-0.041	-0.218
83	-0.208	-0.204	-0.117	-0.108	-0.069	-0.040	-0.039	-0.044	-0.044	-0.205
84	-0.002	-0.033	-0.083	-0.113	-0.190	-0.301	-0.351	-0.406	-0.463	-0.513
85	-0.011	-0.037	-0.076	-0.114	-0.145	-0.235	-0.311	-0.406	-0.478	-0.513
86	-0.088	-0.109	-0.136	-0.175	-0.177	-0.209	-0.260	-0.320	-0.389	-0.470
87	-0.178	-0.197	-0.221	-0.248	-0.277	-0.283	-0.318	-0.343	-0.396	-0.446
88	-0.177	-0.193	-0.207	-0.213	-0.225	-0.244	-0.273	-0.290	-0.328	-0.368
89	-0.198	-0.170	-0.079	-0.009	-0.284	-0.241	-0.243	-0.134	-0.051	-0.309
90	-0.111	-0.139	-0.086	-0.013	-0.087	-0.186	-0.291	-0.307	-0.407	-0.479
91	-0.169	-0.206	-0.110	-0.048	-0.091	-0.009	-0.090	-0.179	-0.269	-0.330
92	-0.228	-0.251	-0.268	-0.198	-0.187	-0.033	-0.099	-0.144	-0.218	-0.283
93	-0.297	-0.298	-0.208	-0.139	-0.091	-0.083	0.060	0.143	0.204	0.275
94	-0.234	-0.217	-0.186	-0.147	-0.112	-0.076	-0.084	0.035	0.083	0.139
95	-0.252	-0.241	-0.228	-0.203	-0.184	-0.198	-0.114	-0.078	-0.019	0.030
96	-0.264	-0.245	-0.225	-0.207	-0.188	-0.162	-0.114	-0.055	0.003	0.037
97	-0.288	-0.213	-0.204	-0.195	-0.183	-0.156	-0.110	-0.065	-0.027	0.020
98	-0.289	-0.218	-0.203	-0.198	-0.186	-0.162	-0.118	-0.075	-0.035	0.008

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TABLE IV.- CONTINUED  
(c) Basic model,  $M = 1.7$

Office No	Angle of attack										Office No	Angle of attack									
	-3°	-1°	0°	1°	2°	4°	6°	8°	10°	12°		-3°	-1°	0°	1°	2°	4°	6°	8°	10°	12°
0	1.561	1.587	1.598	1.571	1.595	1.601	1.588	1.577	1.557	1.543	35	-0.063	-0.056	-0.034	-0.012	0.006	0.046	0.097	0.136	0.176	0.224
1	---	---	---	---	---	---	---	---	---	---	36	-0.061	-0.070	-0.051	-0.024	-0.015	0.034	0.073	0.112	0.152	0.204
2	-.707	-.457	-.439	-.405	-.376	-.334	-.291	-.246	-.207	-.167	37	-0.134	-.127	-.115	-.095	-.072	-.044	-.006	-.069	-.071	-.114
3	-.419	-.379	-.356	-.324	-.302	-.264	-.224	-.188	-.152	-.115	38	-.198	-.197	-.191	-.177	-.165	-.150	-.119	-.095	-.067	-.035
4	-.489	-.436	-.417	-.380	-.356	-.322	-.277	-.243	-.203	-.167	39	-.178	-.110	-.090	-.050	-.016	-.031	-.091	-.147	-.202	-.252
5	-.631	-.581	-.561	-.521	-.500	-.466	-.415	-.365	-.322	-.281	40	-.040	-.011	-.032	-.068	-.100	-.135	-.181	-.218	-.255	-.297
6	-.190	-.156	-.144	-.118	-.097	-.079	-.040	-.010	-.018	-.041	41	-.011	-.064	-.093	-.120	-.146	-.179	-.224	-.261	-.290	-.317
7	-.124	-.150	-.162	-.175	-.189	-.197	-.219	-.230	-.245	-.249	42	-.023	-.036	-.067	-.110	-.142	-.181	-.227	-.266	-.304	-.337
8	-.080	-.065	-.099	-.113	-.131	-.103	-.051	-.025	-.003	-.008	43	-.042	-.009	-.001	-.051	-.143	-.146	-.198	-.248	-.282	-.316
9	-.053	-.026	-.039	-.044	-.046	-.049	-.051	-.053	-.055	-.053	44	-.066	-.054	-.067	-.080	-.090	-.114	-.137	-.164	-.194	-.202
10	-.055	-.030	-.037	-.033	-.024	-.016	-.010	-.026	-.058	-.087	45	-.028	-.062	-.068	-.090	-.108	-.122	-.147	-.170	-.186	-.261
11	---	---	---	---	---	---	---	---	---	---	46	-.026	-.051	-.064	-.079	-.088	-.113	-.134	-.152	-.173	-.219
12	-.207	-.380	-.263	-.289	-.307	-.361	-.414	-.420	-.422	-.476	47	---	---	---	---	---	---	---	---	---	---
13	-.013	-.028	-.047	-.068	-.076	-.116	-.158	-.196	-.240	-.283	48	-.018	-.048	-.062	-.078	-.096	-.114	-.138	-.156	-.171	-.192
14	-.005	-.007	-.020	-.038	-.050	-.079	-.118	-.149	-.187	-.226	49	-.060	-.034	-.004	-.059	-.098	-.195	-.295	-.366	-.441	-.513
15	-.195	-.179	-.176	-.166	-.161	-.165	-.169	-.168	-.175	-.188	50	---	---	---	---	---	---	---	---	---	---
16	-.019	-.016	-.005	-.020	-.029	-.063	-.112	-.148	-.194	-.240	51	---	---	---	---	---	---	---	---	---	---
17	-.725	-.661	-.638	-.599	-.575	-.512	-.407	-.389	-.322	-.222	52	-.150	-.114	-.074	-.036	-.018	-.035	-.103	-.157	-.219	-.263
18	-.198	-.144	-.120	-.101	-.066	-.046	-.041	-.075	-.103	-.143	53	-.063	-.083	-.066	-.037	-.019	-.035	-.097	-.137	-.185	-.244
19	---	---	---	---	---	---	---	---	---	---	54	-.127	-.113	-.095	-.072	-.058	-.033	-.043	-.082	-.129	-.179
20	-.073	-.113	-.126	-.148	-.172	-.196	-.219	-.241	-.266	-.288	55	-.123	-.112	-.096	-.073	-.059	-.021	-.024	-.065	-.109	-.153
21	-.036	-.071	-.085	-.108	-.131	-.158	-.190	-.217	-.246	-.273	56	---	---	---	---	---	---	---	---	---	---
22	-.069	-.037	-.030	-.016	-.004	-.019	-.045	-.072	-.102	-.148	57	-.049	-.070	-.071	-.059	-.056	-.031	-.006	-.041	-.080	-.128
23	-.053	-.021	-.038	-.008	-.027	-.039	-.065	-.088	-.109	-.131	58	-.123	-.121	-.109	-.085	-.073	-.044	-.003	-.040	-.075	-.121
24	-.054	-.024	-.008	-.003	-.022	-.034	-.057	-.078	-.104	-.124	59	-.221	-.157	-.126	-.085	-.045	-.021	-.091	-.161	-.221	-.264
25	-.045	-.008	-.001	-.015	-.029	-.043	-.069	-.092	-.115	-.140	60	-.060	-.005	-.018	-.057	-.088	-.130	-.184	-.230	-.276	-.312
26	---	---	---	---	---	---	---	---	---	---	61	-.011	-.057	-.086	-.113	-.140	-.179	-.220	-.259	-.293	-.321
27	---	---	---	---	---	---	---	---	---	---	62	-.005	-.058	-.096	-.128	-.152	-.196	-.235	-.269	-.294	-.322
28	-.123	-.146	-.151	-.161	-.176	-.185	-.203	-.217	-.234	-.254	63	-.020	-.040	-.073	-.116	-.145	-.183	-.239	-.278	-.296	-.341
29	-.037	-.002	-.048	-.124	-.160	-.250	-.318	-.379	-.450	-.547	64	-.019	-.020	-.041	-.094	-.134	-.178	-.224	-.287	-.301	-.326
30	-.128	-.160	-.129	-.097	-.076	-.087	-.095	-.111	-.134	-.164	65	-.035	-.073	-.072	-.095	-.120	-.177	-.225	-.266	-.293	-.318
31	-.171	-.156	-.129	-.085	-.060	-.013	-.042	-.085	-.122	-.166	66	-.092	-.086	-.094	-.112	-.118	-.168	-.217	-.244	-.276	-.300
32	-.046	-.039	-.021	-.005	-.004	-.033	-.075	-.109	-.150	-.196	67	---	---	---	---	---	---	---	---	---	---
33	-.048	-.032	-.019	-.009	-.025	-.061	-.112	-.154	-.197	-.248	68	-.077	-.096	-.103	-.119	-.126	-.169	-.222	-.233	-.251	-.282
34	-.056	-.041	-.030	-.008	-.005	-.054	-.099	-.140	-.180	-.243	69	-.024	-.054	-.080	-.097	-.113	-.135	-.158	-.176	-.205	-.232
34A	-.071	-.054	-.045	-.005	-.001	-.048	-.097	-.141	-.181	-.235	70	---	---	---	---	---	---	---	---	---	---

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Office No	Angle of attack									
	-3°	-1°	0°	1°	2°	4°	6°	8°	10°	12°
71	---	---	---	---	---	---	---	---	---	---
72	-.0187	-.0158	-.0131	-.0071	-.0041	0.0023	0.100	0.168	0.241	0.349
73	-.174	-.141	-.108	-.051	-.020	-.045	-.111	-.171	-.236	-.304
74	---	---	---	---	---	---	---	---	---	---
75	-.157	-.126	-.106	-.073	-.055	-.016	-.048	-.091	-.144	-.199
76	-.128	-.124	-.115	-.085	-.072	-.036	-.019	-.069	-.113	-.166
77	-.141	-.132	-.132	-.109	-.097	-.062	-.003	-.036	-.087	-.140
78	-.109	-.107	-.102	-.077	-.056	-.017	-.036	-.071	-.112	-.158
79	-.142	-.140	-.137	-.110	-.098	-.070	-.021	-.018	-.060	-.108
80	-.149	-.145	-.134	-.111	-.099	-.071	-.027	-.008	-.052	-.089
81	-.278	-.203	-.160	-.119	-.066	-.021	-.120	-.191	-.271	-.308
82	-.074	-.019	-.013	-.047	-.082	-.135	-.196	-.241	-.285	-.330
83	-.010	-.041	-.076	-.098	-.138	-.175	-.243	-.274	-.313	-.351
84	0	-.055	-.091	-.111	-.150	-.193	-.250	-.280	-.314	-.352
85	-.017	-.052	-.092	-.118	-.148	-.187	-.242	-.298	-.325	-.365
86	-.005	-.044	-.083	-.133	-.174	-.220	-.287	-.316	-.347	-.387
87	-.065	-.097	-.115	-.139	-.184	-.231	-.278	-.313	-.340	-.364
88	-.089	-.110	-.123	-.135	-.173	-.227	-.270	-.305	-.334	-.356
89	-.094	-.111	-.121	-.129	-.154	-.209	-.263	-.289	-.301	-.321
90	-.042	-.018	-.058	-.137	-.185	-.263	-.306	-.410	-.476	-.532
91	-.136	-.111	-.068	-.014	-.010	-.089	-.091	-.223	-.287	-.356
92	-.184	-.146	-.123	-.070	-.043	-.020	-.077	-.173	-.242	-.309
93	-.185	-.163	-.124	-.074	-.039	-.019	-.056	-.172	-.235	-.299
94	-.141	-.140	-.129	-.081	-.054	-.017	-.027	-.111	-.166	-.226
95	-.187	-.165	-.151	-.112	-.096	-.068	-.022	-.012	-.056	-.091
96	-.193	-.173	-.166	-.118	-.088	-.068	-.029	-.015	-.059	-.117
97	-.189	-.164	-.155	-.130	-.119	-.091	-.033	-.004	-.036	-.084
98	-.174	-.163	-.156	-.132	-.120	-.094	-.041	-.019	-.044	-.067

TABLE IV.- CONTINUED  
(d) Model with rocket packets,  $M = 1.2$

Orifice No.	Angle of attack					Orifice No.	Angle of attack					Orifice No.	Angle of attack				
	-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°
0	1.360	1.375	1.384	1.371	1.384	34	----	----	----	----	----	67	----	----	----	----	----
1	----	----	----	----	----	34A	-.014	.082	.176	.299	.363	68	-.083	-.166	-.246	-.365	-.504
2	.485	.395	.287	.193	.107	35	-.103	-.048	.042	.133	.194	69	-.055	-.151	-.207	-.316	-.407
3	.401	.310	.218	.132	.057	36	-.230	-.164	-.042	.033	.168	70	----	----	----	----	----
4	.608	.569	.436	.307	.212	37	-.248	-.175	-.095	-.019	.032	71	----	----	----	----	----
5	.552	.477	.398	.320	.253	38	-.356	-.333	-.276	-.220	-.198	72	-.368	-.255	-.046	.170	.247
6	-.034	-.094	-.154	-.204	-.250	39	.159	-.123	-.497	-.704	-.745	73	-.347	-.221	-.128	.050	.334
7	-.379	-.426	-.441	.408	-.418	40	.012	-.189	-.506	-.690	-.729	74	----	----	----	----	----
8	.106	.091	.081	.051	.055	41	.033	-.122	-.430	-.644	-.702	75	-.210	-.121	-.008	.091	.149
9	----	----	----	----	----	42	.030	-.094	-.212	-.560	-.673	76	-.201	-.133	-.037	.042	.107
10	.049	-.013	-.080	-.126	-.174	43	-.016	-.112	-.222	-.382	-.646	77	-.163	-.152	-.073	.004	.068
11	----	----	----	----	----	44	-.064	-.155	-.255	-.310	-.333	78	-.173	-.115	-.034	.043	.086
12	.114	.193	.309	.424	.530	45	-.085	-.151	-.227	-.289	-.305	79	-.185	-.151	-.079	-.012	.065
13	-.060	-.036	.060	.137	.245	46	-.059	-.134	-.213	-.267	-.306	80	-.134	-.149	-.113	-.044	.101
14	-.073	-.030	.047	.134	.201	47	----	----	----	----	----	81	.162	-.146	-.577	-.726	-.727
15	.226	.234	.256	.263	.271	48	-.018	-.138	-.194	-.254	-.287	82	.003	-.252	-.576	-.704	-.720
16	.003	.059	.174	.271	.308	49	-.117	.065	.268	.384	.517	83	-.038	-.220	-.557	-.692	-.709
17	.505	.328	.153	-.031	-.162	50	----	----	----	----	----	84	-.025	-.170	-.458	-.619	-.682
18	.013	-.153	-.345	-.474	-.575	51	----	----	----	----	----	85	-.040	-.144	-.304	-.527	-.644
19	----	----	----	----	----	52	-.307	-.209	-.058	.164	.299	86	-.110	-.210	-.296	-.445	-.579
20	-.141	-.250	-.381	-.496	-.593	53	-.367	-.243	-.020	.116	.167	87	-.207	-.301	-.373	-.445	-.562
21	.034	-.060	-.135	-.227	-.397	54	-.177	-.108	0	.085	.158	88	-.167	-.244	-.297	-.337	-.511
22	.082	.007	-.080	-.167	-.247	55	-.173	-.126	-.049	.015	.071	89	-.109	-.209	-.244	-.276	.493
23	.058	-.016	-.108	-.182	-.256	56	----	----	----	----	----	90	-.297	-.060	.212	.387	.476
24	.044	-.034	-.108	-.183	-.250	57	-.157	-.103	-.029	.033	.050	91	-.363	-.166	.011	.186	.351
25	.051	-.035	-.125	-.203	-.265	58	-.185	-.157	-.083	-.005	.052	92	-.365	-.247	-.049	.203	.310
26	----	----	----	----	----	59	.129	-.168	-.610	-.753	-.753	93	-.351	-.213	.007	.206	.275
27	----	----	----	----	----	60	.002	-.246	-.577	-.715	-.752	94	-.251	-.110	.056	.135	.169
28	-.305	-.337	-.336	-.220	-.239	61	-.019	-.210	-.558	-.701	-.729	95	-.251	-.201	-.123	-.041	.017
29	-.400	-.285	-.045	.183	.408	62	-.027	-.143	-.287	-.653	-.708	96	-.252	-.188	-.131	-.051	.004
30	-.394	-.270	-.063	.133	.217	63	-.030	-.139	-.272	-.581	-.668	97	-.202	-.169	-.129	-.050	.025
31	-.155	-.087	-.012	.096	.244	64	-.061	-.157	-.271	-.518	-.642	98	-.147	-.166	-.146	-.067	.002
32	.224	.244	.290	.326	.357	65	-.105	-.203	-.313	-.475	-.635						
33	-.343	-.285	-.134	.039	.087	66	-.131	-.197	-.301	-.417	-.560						



TABLE IV.- CONTINUED  
(e) Model with rocket packets,  $M = 1.3$

Orifice No.	Angle of attack					Orifice No.	Angle of attack					Orifice No.	Angle of attack				
	-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°
0	1.417	1.442	1.440	1.428	1.407	34	---	---	---	---	---	67	---	---	---	---	---
1	---	---	---	---	---	34A	.047	.012	.124	.245	.395	68	-.099	-.139	-.210	-.262	-.414
2	.508	.431	.321	.228	.151	35	-.093	-.046	.041	.134	.236	69	-.060	-.115	-.175	-.226	-.315
3	.419	.346	.247	.163	.083	36	-.209	-.162	-.075	.026	.135	70	---	---	---	---	---
4	.640	.522	.377	.278	.205	37	-.258	-.220	-.128	-.030	.047	71	---	---	---	---	---
5	.585	.518	.417	.337	.266	38	-.320	-.309	-.269	-.222	-.156	72	-.310	-.226	-.092	.146	.268
6	.040	-.012	-.053	-.128	-.176	39	.128	-.023	-.255	-.434	-.551	73	-.325	-.233	-.084	.003	.209
7	-.293	-.334	-.378	-.396	-.371	40	.043	-.105	-.303	-.453	-.550	74	---	---	---	---	---
8	-.020	.057	.065	.081	.055	41	-.011	-.061	-.267	-.444	-.544	75	-.226	-.141	-.040	.082	.178
9	---	---	---	---	---	42	-.008	-.054	-.154	-.355	-.507	76	-.210	-.155	-.065	.038	.125
10	.054	.009	-.050	-.101	-.155	43	.003	-.065	-.155	-.296	-.431	77	-.209	-.171	-.084	.015	.089
11	---	---	---	---	---	44	-.068	-.127	-.204	-.273	-.381	78	-.176	-.124	-.043	.051	.123
12	.143	.226	.325	.445	.561	45	-.084	-.126	-.200	-.265	-.277	79	-.195	-.156	-.075	-.003	.054
13	-.055	-.004	.066	.158	.265	46	-.050	-.107	-.182	-.235	-.256	80	-.194	-.162	-.092	-.035	.024
14	-.055	-.011	.052	.132	.225	47	---	---	---	---	---	81	.180	-.034	-.285	-.453	-.565
15	.220	.231	.232	.252	.267	48	-.062	-.106	-.172	-.238	-.268	82	-.024	-.136	-.348	-.485	-.567
16	-.046	-.009	.085	.231	.348	49	-.226	.023	.209	.358	.446	83	-.016	-.141	-.358	-.500	-.578
17	.580	.450	.288	.125	-.027	50	---	---	---	---	---	84	.004	-.098	-.315	-.466	-.562
18	.060	-.054	-.192	-.315	-.419	51	---	---	---	---	---	85	-.012	-.086	-.246	-.425	-.524
19	---	---	---	---	---	52	-.274	-.172	-.025	.085	.292	86	-.085	-.138	-.208	-.350	-.464
20	-.139	-.218	-.312	-.409	-.487	53	-.324	-.299	-.170	.053	.183	87	-.174	-.228	-.282	-.358	-.464
21	-.027	-.089	-.196	-.291	-.397	54	-.175	-.115	-.036	.072	.170	88	-.173	-.209	-.229	-.298	-.415
22	.071	.018	-.065	-.137	-.202	55	-.177	-.136	-.064	.021	.095	89	-.140	-.191	-.223	-.238	-.390
23	.054	.005	-.082	-.150	-.209	56	---	---	---	---	---	90	-.227	-.045	.174	.357	.465
24	.041	-.005	-.082	-.150	-.207	57	-.126	-.131	-.087	-.015	.061	91	-.311	-.192	-.013	.154	.300
25	.026	-.020	-.096	-.163	-.219	58	-.173	-.159	-.095	-.017	.062	92	-.321	-.218	-.062	.067	.325
26	---	---	---	---	---	59	.169	-.050	-.316	-.483	-.590	93	-.307	-.236	-.087	.138	.304
27	---	---	---	---	---	60	.025	-.151	-.369	-.511	-.592	94	-.267	-.229	-.086	.073	.193
28	-.260	-.296	-.337	-.408	-.412	61	.006	-.114	-.316	-.468	-.561	95	-.284	-.212	-.136	-.044	.032
29	-.313	-.227	-.019	.214	.443	62	.008	-.093	-.314	-.462	-.559	96	-.266	-.208	-.135	-.042	.032
30	-.345	-.353	-.239	-.036	.190	63	-.008	-.093	-.180	-.418	-.528	97	-.235	-.190	-.131	-.045	.031
31	-.235	-.089	-.030	.062	.171	64	-.042	-.102	-.178	-.348	-.467	98	-.216	-.189	-.134	-.062	.006
32	.230	.283	.327	.361	.397	65	-.095	-.142	-.218	-.322	-.457						
33	-.348	-.303	-.207	-.052	.134	66	-.114	-.158	-.228	-.301	-.418						

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TABLE IV.- CONCLUDED  
(f) Model with rocket packets,  $M = 1.7$

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Orifice No.	Angle of attack					Orifice No.	Angle of attack					Orifice No.	Angle of attack				
	-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°		-3°	0°	4°	8°	12°
0	1.573	1.584	1.566	1.578	1.535	33	-.141	-.150	-.115	-.045	.056	65	-.033	-.081	-.168	-.238	-.292
1	---	---	---	---	---	34	---	---	---	---	---	66	-.048	-.084	-.175	-.221	-.276
2	.306	.433	.338	.255	.175	34A	-.026	-.018	.017	.162	.249	67	---	---	---	---	---
3	.420	.351	.263	.190	.119	35	.046	-.029	.049	.166	.271	68	-.063	-.103	-.186	-.219	-.265
4	.489	.413	.314	.241	.172	36	-.039	-.021	.045	.114	.201	69	.019	-.069	-.121	-.163	-.203
5	.633	.556	.454	.367	.285	37	-.171	-.166	-.114	-.044	.060	70	---	---	---	---	---
6	.195	.141	.074	.021	-.030	38	-.183	-.186	-.155	-.101	-.038	71	---	---	---	---	---
7	-.117	-.152	-.186	-.218	-.236	39	-.176	.086	-.029	-.139	-.233	72	-.146	-.146	-.059	.115	.275
8	-.062	-.105	-.087	-.030	.006	40	.036	-.032	-.119	-.193	-.262	73	-.215	-.151	-.003	.094	.238
9	---	---	---	---	---	41	-.014	-.089	-.165	-.238	-.294	74	---	---	---	---	---
10	.056	.038	.017	-.023	-.079	42	.028	-.073	-.167	-.245	-.310	75	-.107	-.084	-.015	.072	.193
11	---	---	---	---	---	43	.050	-.008	-.128	-.220	-.290	76	-.117	-.117	-.057	.054	.141
12	.208	.258	.360	.467	.470	44	-.023	-.069	-.115	-.162	-.269	77	-.138	-.137	-.051	.030	.112
13	.017	.047	.111	.191	.246	45	-.026	-.077	-.125	-.163	-.246	78	-.114	-.098	-.015	.058	.144
14	.004	0	.072	.140	.227	46	-.020	-.064	-.112	-.150	-.201	79	-.136	-.120	-.066	.003	.089
15	.193	.124	.170	.173	.189	47	---	---	---	---	---	80	-.137	-.123	-.078	-.003	.086
16	-.040	-.026	.044	.115	.204	48	-.014	-.063	-.113	-.148	-.181	81	.247	.133	.004	-.156	-.254
17	.723	.636	.488	.391	.222	49	-.029	.009	.157	.365	.490	82	.057	-.023	-.102	-.220	-.292
18	.199	.128	.046	-.046	-.128	50	---	---	---	---	---	83	.003	-.076	-.168	-.247	-.312
19	---	---	---	---	---	51	---	---	---	---	---	84	-.002	-.084	-.170	-.252	-.312
20	-.090	-.146	-.182	-.229	-.269	52	-.006	.026	.090	.213	.383	85	.015	-.083	-.164	-.232	-.295
21	-.026	-.105	-.149	-.210	-.254	53	-.212	-.185	-.105	-.003	.093	86	-.028	-.082	-.181	-.256	-.302
22	.075	.035	-.016	-.071	-.151	54	-.091	-.052	-.016	.081	.175	87	-.069	-.120	-.206	-.276	-.329
23	.054	.005	-.059	-.089	-.135	55	-.098	-.092	-.030	.045	.143	88	-.088	-.123	-.207	-.277	-.330
24	.053	.010	-.059	-.089	-.131	56	---	---	---	---	---	89	-.089	-.124	-.198	-.267	-.296
25	.036	-.008	-.059	-.107	-.144	57	-.010	-.045	-.025	.027	.103	90	.005	.079	.212	.328	.458
26	---	---	---	---	---	58	-.114	-.105	-.049	.026	.113	91	-.100	-.083	.020	.164	.318
27	---	---	---	---	---	59	.221	.115	-.035	-.175	-.270	92	.159	-.133	.006	.128	.285
28	-.113	-.148	-.168	-.215	-.249	60	.062	-.027	-.126	-.223	-.299	93	-.166	-.119	.012	.108	.247
29	-.027	.060	.237	.376	.640	61	-.005	-.077	-.163	-.241	-.301	94	-.100	-.107	-.052	.051	.187
30	-.081	-.097	.046	.080	.274	62	.004	-.081	-.178	-.249	-.303	95	-.155	-.143	-.080	-.011	.089
31	-.146	-.113	.046	.077	.154	63	.023	-.071	-.172	-.253	-.313	96	-.165	-.146	-.086	-.048	.108
32	-.008	-.007	.096	.346	.490	64	.008	-.056	-.155	-.238	-.293	97	-.156	-.143	-.098	.011	.073
												98	-.155	-.148	-.106	-.029	.051

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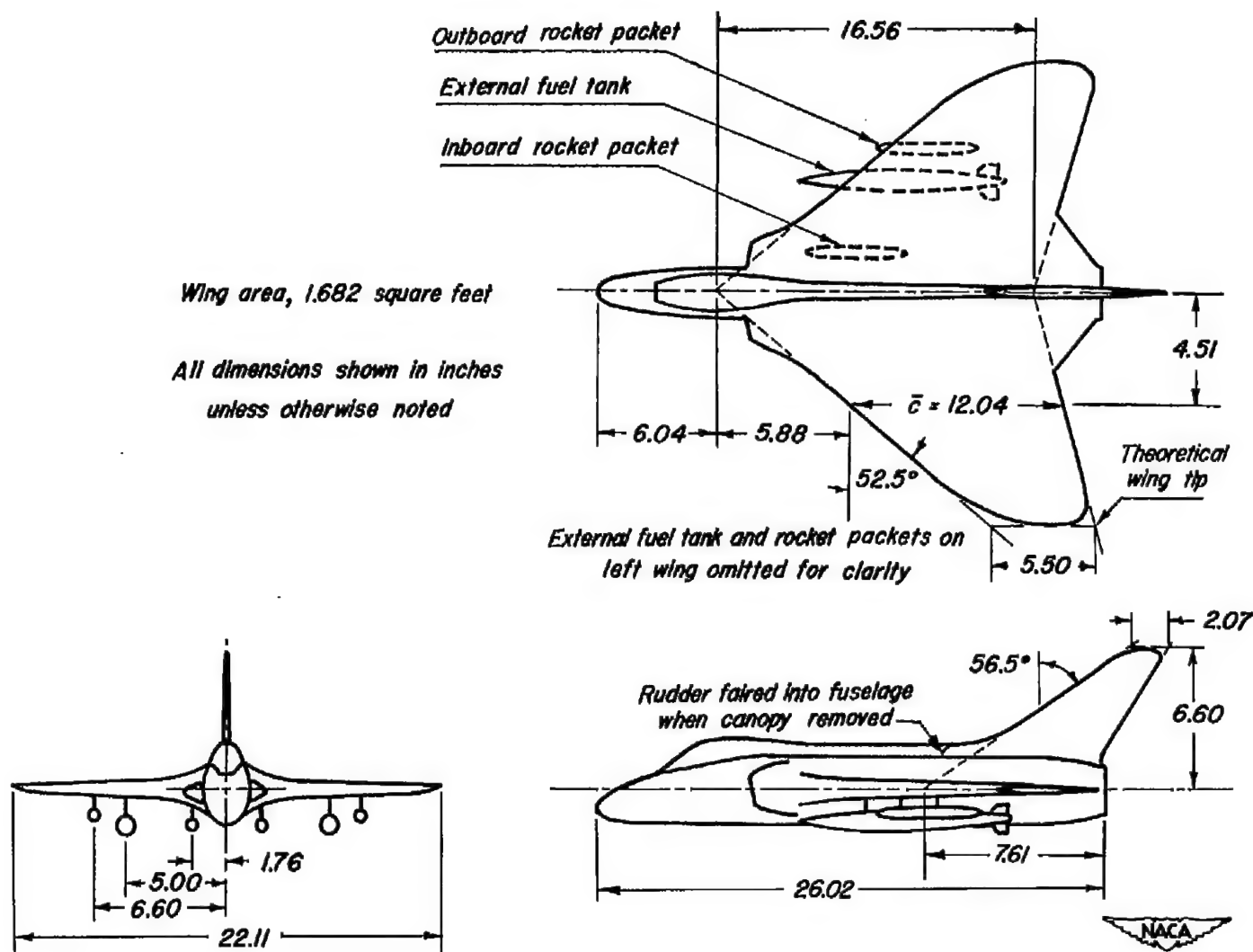


Figure 1.—Three-view drawing of the model showing the external fuel tanks and rocket packets.

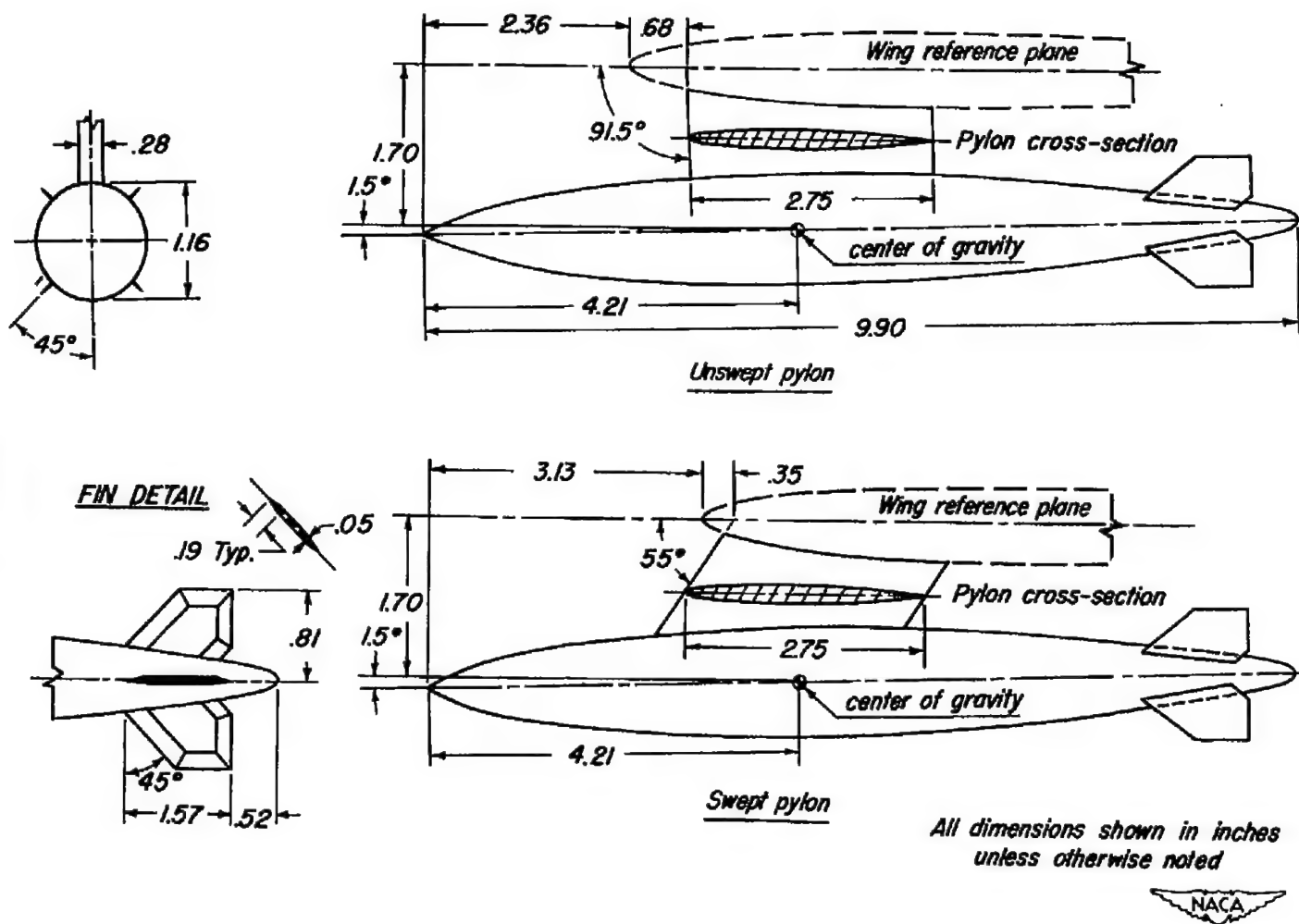
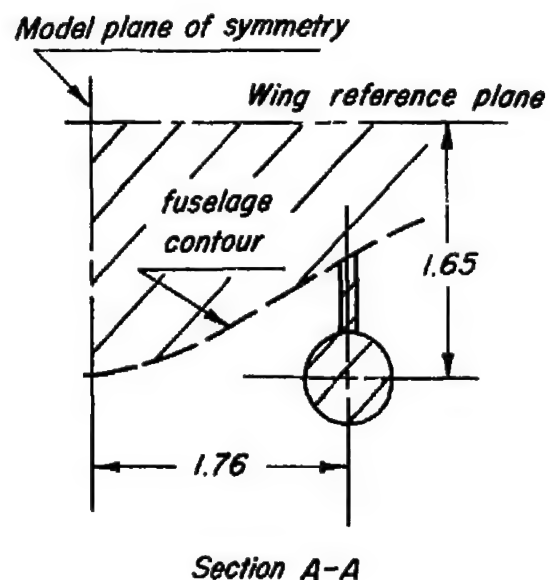
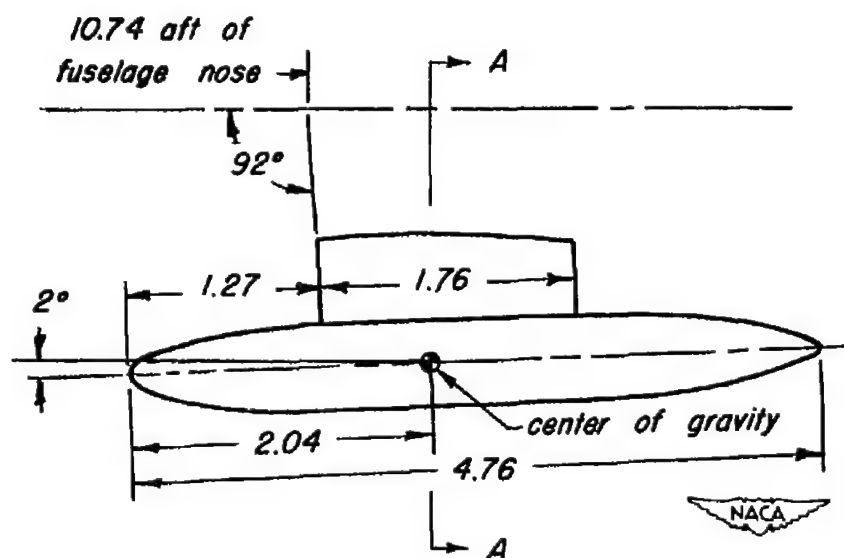


Figure 2.-Details of the external fuel tanks with unswept and swept pylons.





All dimensions shown in inches  
unless otherwise noted



(b) Inboard location.

Figure 3. — Concluded.

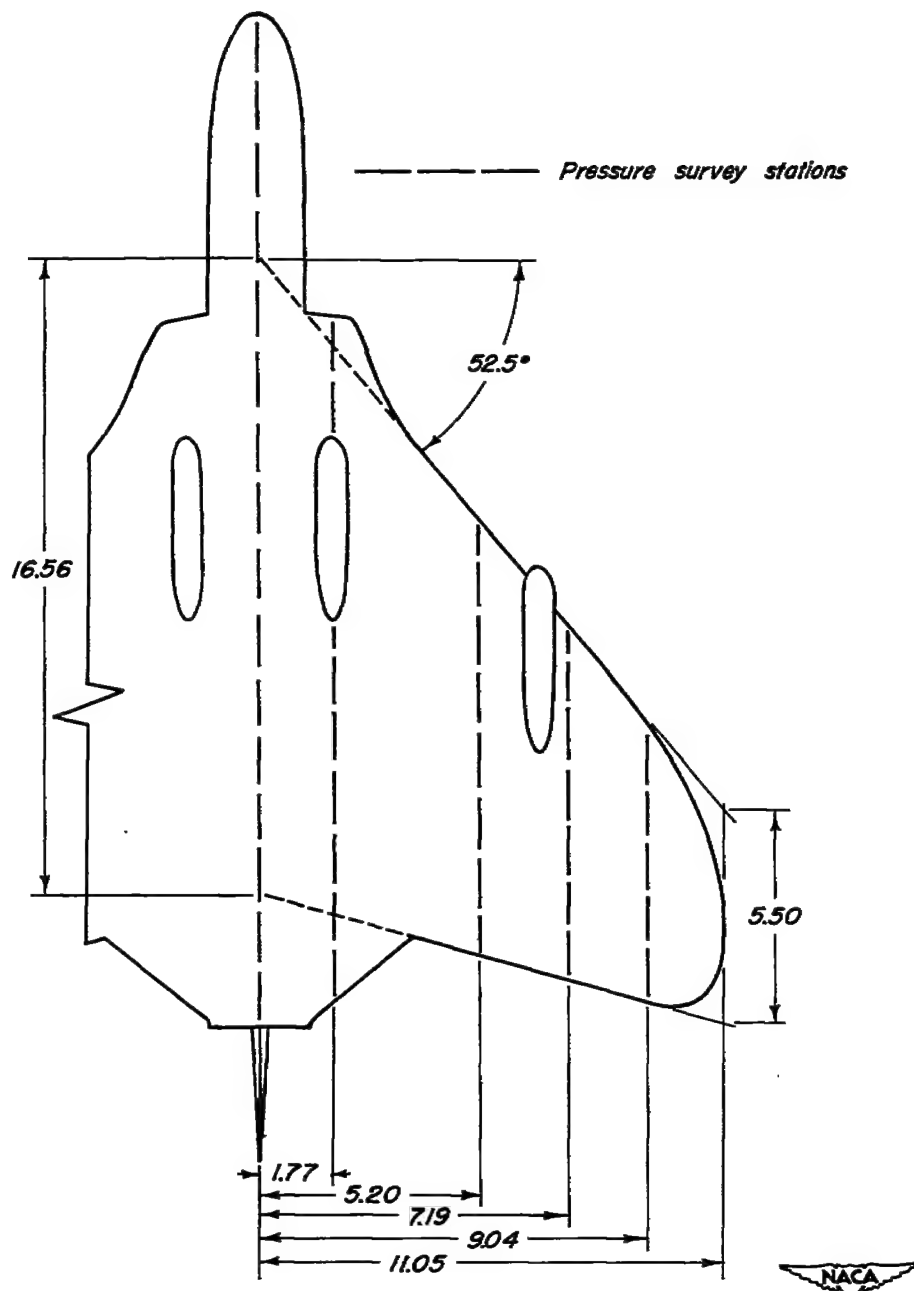


Figure 4.—Dimensional sketch of the lower surface of the model with rocket packets installed, showing the pressure survey station.

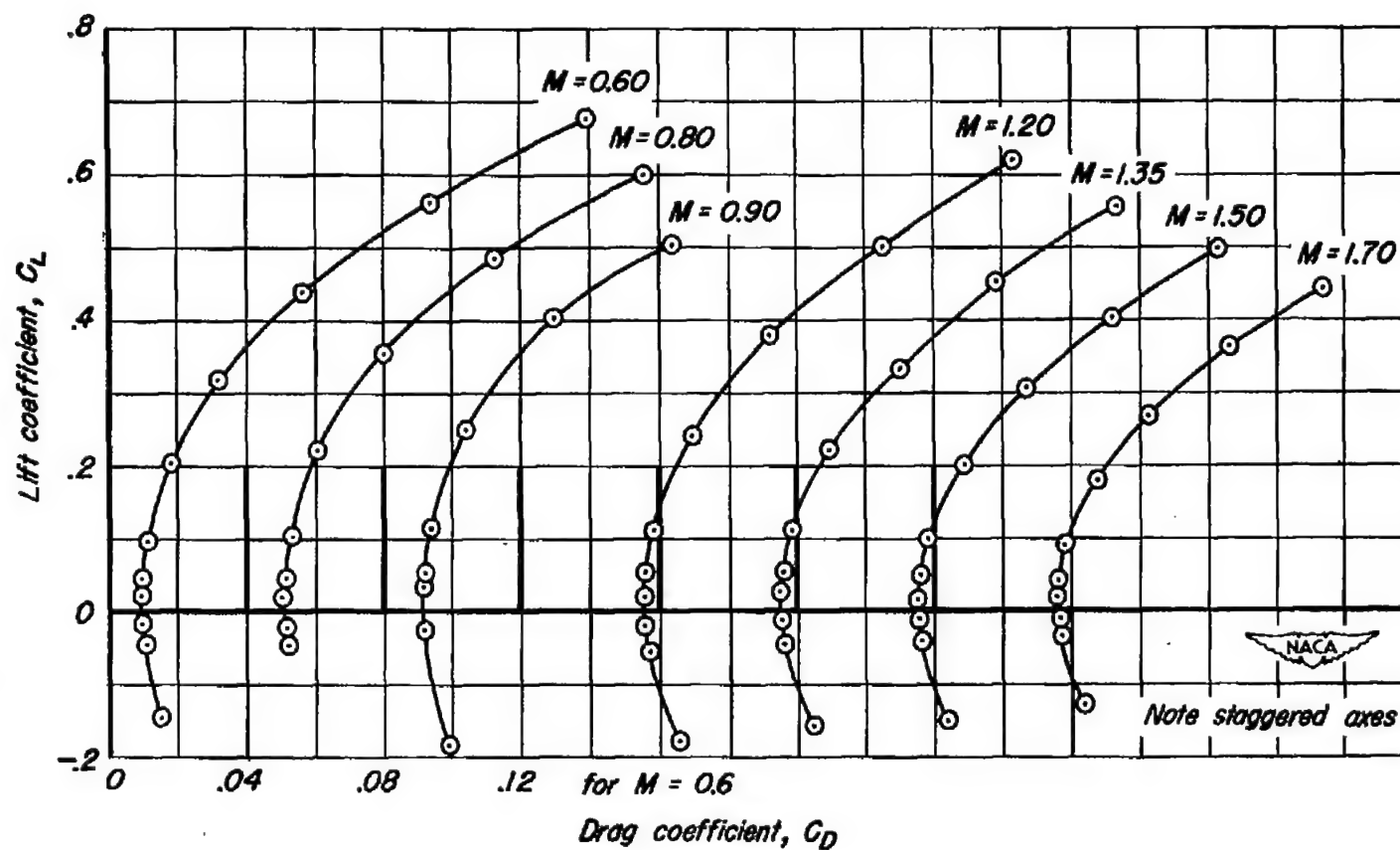


Figure 5.- Variation of drag coefficient with lift coefficient for the basic model.

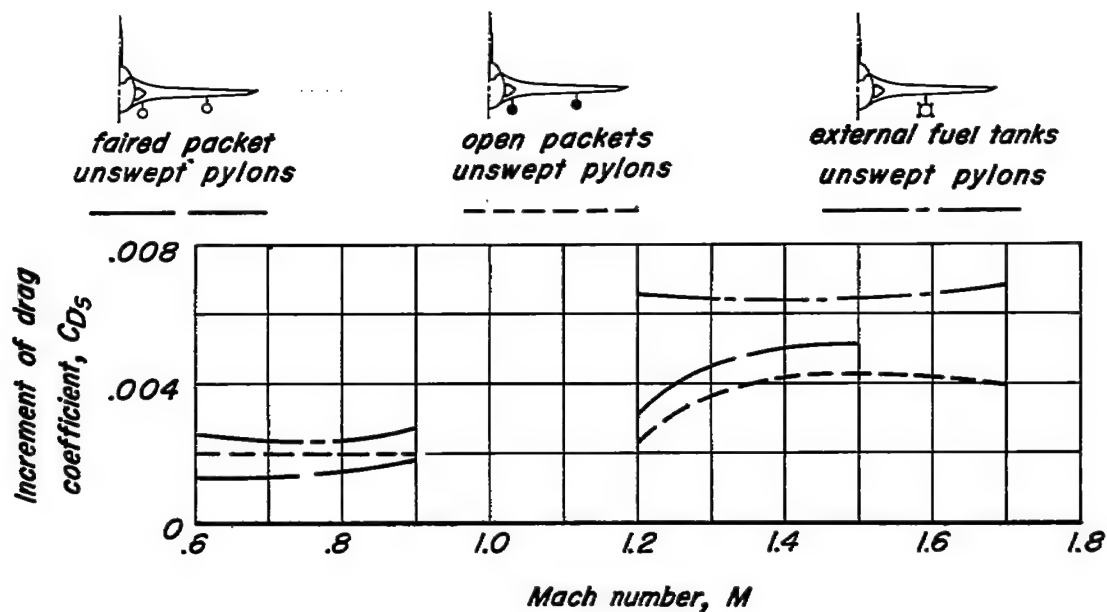
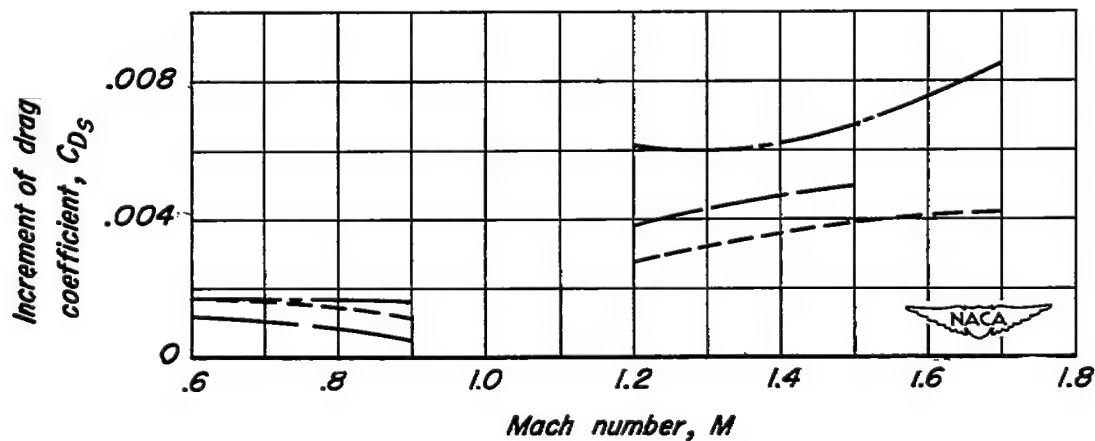
(a)  $C_L = 0$ (b)  $C_L = 0.25$ 

Figure 6.- Variation of Increment of drag coefficient with Mach number at 0 and 0.25 lift coefficient for the various external store configurations mounted on the model.

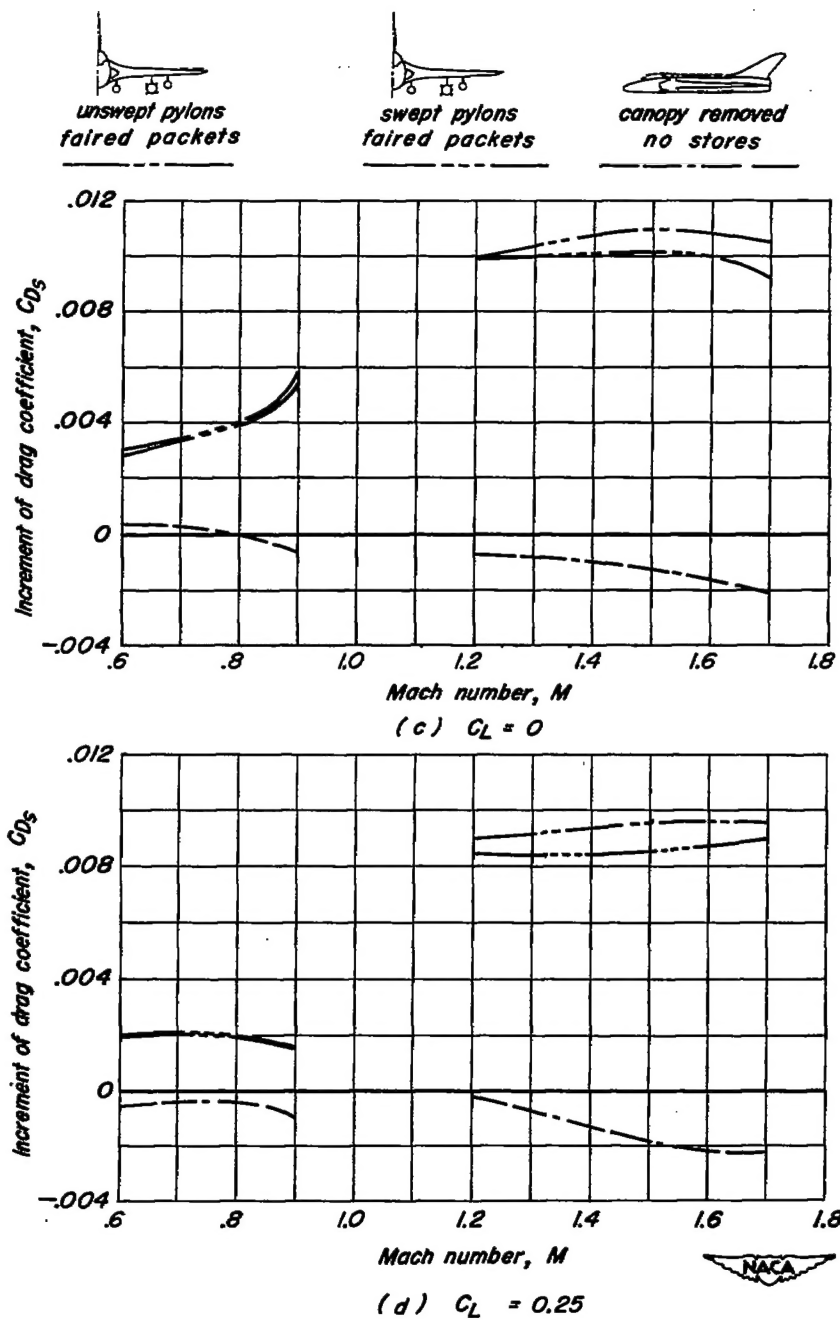


Figure 6.- Concluded.

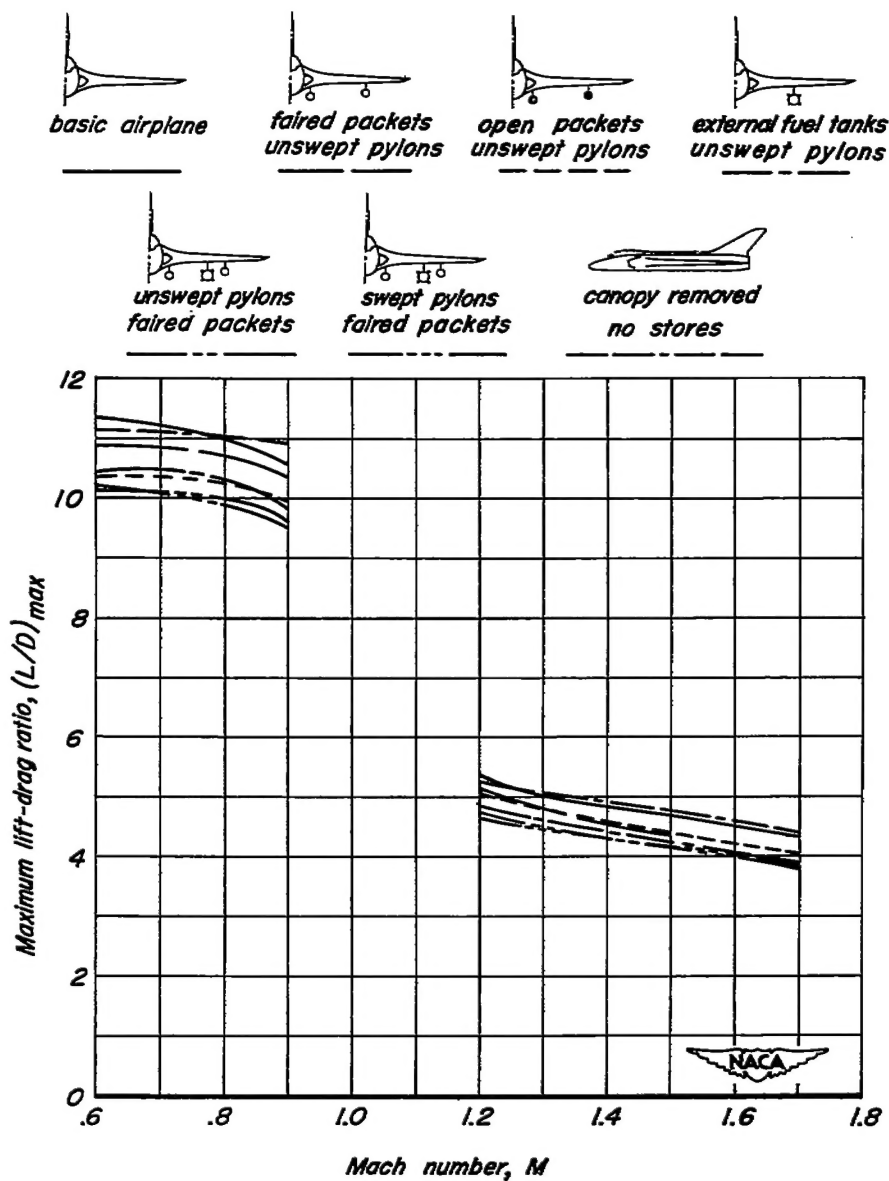


Figure 7.- Variation of the maximum lift-drag ratio with Mach number for the various external store configurations mounted on the model.

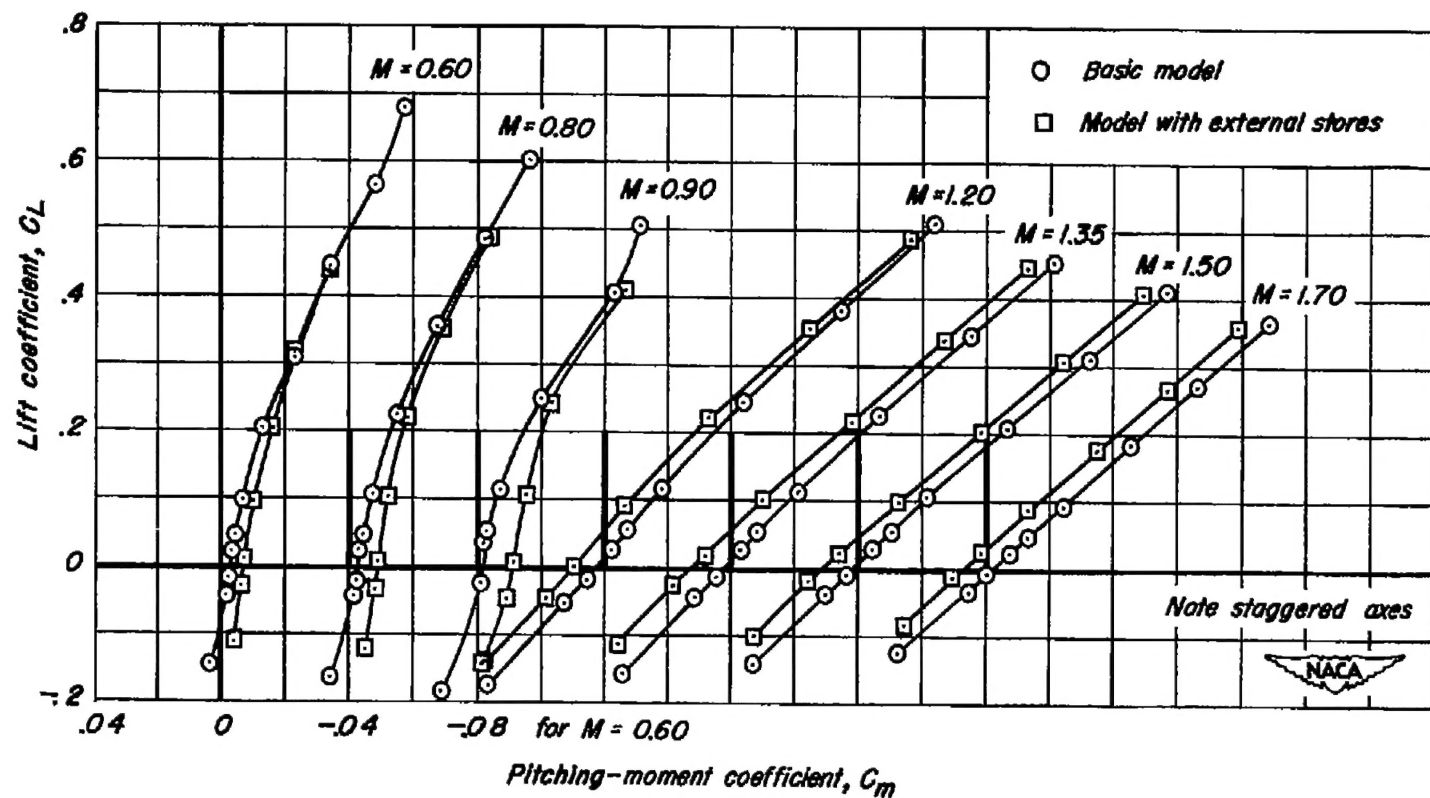


Figure 8.—Variation of pitching-moment coefficient with lift coefficient for the basic model and for the model fitted with two external fuel tanks and four faired rocket packets mounted on unswept pylons.

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